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(71) Applicant: OTI OPHTHALMIC TECHNOLOGIES INC. [CA/CA]; 37 Kodiak Crescent, Unit #16, Downsview, Ontario M3H 3E5 (CA).

(72) Inventors: PODOLEANU, Adrian, Gh.; 73 Kensing Gardens, Canterbury, Kent CT2 7RF (GB). JACKSON, David, A.; Domus, Stodmarsh Road, Canterbury, Kent CT3 4AH (GB).

(74) Agent: HEWSON, Donald, E.; Marks & Clerk, Suite #13, 2145 Dunwin Drive, Mississauga, Ontario L5L 4L9 (CA).

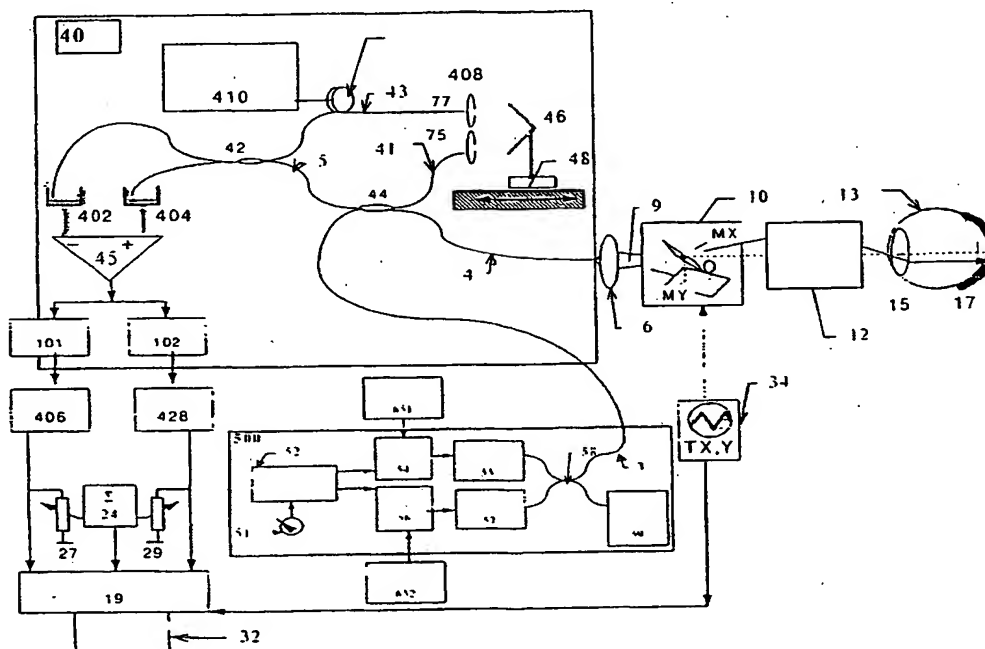
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(54) Title: OPTICAL MAPPING APPARATUS WITH ADJUSTABLE DEPTH RESOLUTION



OPTICAL MAPPING APPARATUS WITH ADJUSTABLE DEPTH RESOLUTION

FIELD OF THE INVENTION:

This invention relates to an optical coherence tomographic apparatus and methods which can be used to supply images with adjustable depth resolution and/or superimposed images with different depth resolution from different objects, with applicability to biological investigations and particularly, but not exclusively, to eye retinal mapping.

BACKGROUND OF THE INVENTION:

This description refers mainly to the eye as the object. This has to be understood as merely a way to help the description and not as a restriction of the application of the present invention. Where "eye" is mentioned, a more general transparent and scattering object may be sought instead.

For eye fundus investigation, visual scientists and ophthalmologists are using scanning laser ophthalmoscopes (SLO), which are confocal imaging systems. A recent advance in depth resolution has been provided by optical coherence tomography (OCT), which has the potential of achieving much better depth resolution, as the limit in this case is not set by the eye any more, but by the coherence length of the source. (Superluminescent diodes and mode-locked lasers are now available with coherence lengths less than 20 μm and 5 μm respectively).

However, due to the low coherence length, the OCT transversal images show only fragments of the retina and are difficult to interpret. In addition, due to the curvature of the retina at the back of the eye lens and due to the angular path variation of the scanned ray, the OCT transversal images show arcs at the extremities of the field investigated when the angular scanned field is larger than, say 6° . For example, for an eye lens of 2 cm focal length, the coherence plane curves in the form of an arc where

at maximum angular deviation, of $\pm 3^\circ$, the distance from the plane is larger than 70 μm , which is much higher than the coherence length of the most super luminescent diodes on the market. These transversal images may be of use for ophthalmologists only if the fragments sampled by the OCT from the fundus are uniquely placed in
5 correspondence with fundus images produced by fundus cameras or with the SLO images. Such a correspondence is even more difficult to implement due to the inadvertent movement of the eye during investigation.

Unlike those provided by OCTs, the images provided by fundus cameras and SLOs are of much coarser depth resolution and they show the overall aspect of the
10 retina. At the present time, the SLO and OCT depth resolutions are in a ratio of more than 10 and the depth resolution of OCT is not adjustable. This makes the appearance of OCT and SLO images very different and their comparison impractical. The OCT is a new tool in the investigative ophthalmology while the SLOs have been in use for at least a decade and have been used extensively in the eye diagnosis.

15 A need exists for procedures to help the interpretation of OCT transversal images and to ease their comparison with the SLO images for which large data bases for diagnostics have been created.

PODOLEANU *et al.* United States patent No. 5,975,697 issued November 2, 1999 shares certain teachings herewith. However, that patent is directed to an optical
20 mapping apparatus which specifically and particularly requires a raster scanning means for transversely scanning an optical output from the interferometer and an analysis means which is coupled to the raster scanner for demodulating a photodetected signal.

The present invention provides an optical mapping apparatus with adjustable depth resolution which comprises an interferometer which may be chosen from the
25 group of fiberized interferometers and bulk interferometers, where the interferometer comprises a first optical path and a second optical path leading to an object location, and to a reference reflecting assembly, respectively. Scanning means are provided for transversely scanning an optical output from the interferometer over a predetermined area, together with interface optics for transferring an optical beam from the scanning
30 means to an object situated at the object location, and for transferring a returned optical

output being reflected and scattered from the object back to the interferometer, along the first optical path. Means for directing at least a portion of the returned optical output beam towards the reference reflecting assembly are included in the optical mapping apparatus, together with means to alter at least one of the first optical path and the second path so as to introduce intensity modulation, or phase modulation, or intensity modulation and phase modulation. The optical mapping apparatus also includes means to alter the length of at least the second optical path in sets or continuously, at a pace synchronized with the transversal scanning means.

In one embodiment of the present invention, the interferometer is excited by an optical radiation source or a source with adjustable coherence length. The apparatus further comprises comparator or an analyzing means, coupled to the scanning means, for comparing a signal representative of the optical beam transferred to the object, with the output signal from the reference reflector assembly, so as to demodulate and produce an output signal from the interferometer. Finally, means for displaying or storing an image of at least part of an object, based on the output signal from the interferometer, are provided.

Another embodiment of the present invention provides an optical mapping apparatus which includes a confocal optical receiver with adjustable focal depth and an optical splitter for internally directing light returned from an object situated at the object location to the confocal optical receiver. Scanning means for transversely scanning an optical output from the interferometer over a predetermined area are provided, together with interface optics for transferring an optical beam from the scanning means to an object and for transferring an optical output beam reflected and scattered from the object back to the optical splitter through the scanning means, and from the optical splitter to both of the interferometer and the confocal optical receiver, in a ratio determined by the optical splitter. Means are provided to alter at least one of the first optical path and the second optical path, to introduce intensity modulation, or phase modulation, or intensity modulation and phase modulation. Means are also provided to alter at least the second optical path, in steps or continuously, at a pace synchronized with the scanning means.

In this alternative embodiment, the interferometer is excited by an optical radiation source or a source with adjustable coherence length. The apparatus further comprises comparator or analyzing means, coupled to the scanning means, for comparing a signal representative of the optical beam transferred to the object, with the output signal from the confocal optical receiver, so as to demodulate and produce an output signal from the interferometer. As well, means for processing an image created by the interferometer and an image created by the confocal optical receiver are provided, together with means for simultaneous display of the respective images created by the interferometer and the confocal optical receiver.

10 In yet another embodiment of the present invention, the interferometer is chosen from the group consisting of fiberized interferometers and bulk interferometers, where the interferometer comprises a first optical path and a second optical path leading to an object location, and to a reference reflector assembly, respectively. An optical element is provided for producing an enlargement of the correlation function
15 of the optical source when placed in either of the first path or the second path. Scanning means are provided for transversely scanning an optical output from the interferometer over a predetermined area, together with interface optics for transferring an optical beam from the scanning means to an object situated at the object location, and for transferring a returned optical output beam reflected and scattered from the
20 object back to the interferometer along the first optical path. Means are provided for directing at least a portion the returned optical beam towards the reference reflector assembly, and means are provided to alter at least one of the first optical path and the second optical path so as to introduce intensity modulation, or phase modulation, or intensity modulation and phase modulation.

25 In this alternative embodiment, the interferometer is excited by an optical source chosen from the group consisting of broad band optical sources and sources having adjustable coherence lengths. The apparatus further comprises comparator or analyzing means coupled to the scanning means, for comparing a signal representative of the optical beam transferred to the object, with the output signal from the reference
30 reflector assembly, so as to demodulate and produce an output signal from the

interferometer. Means are provided for longitudinal scanning, to alter the length of the first optical path or the second optical path in steps or continuously, at a pace synchronized with transversal scanning means. Means are also provided for displaying or storing an image of at least part of the object based on the output signal from the
5 interferometer.

Yet a further embodiment of the present invention comprises at least interferometers. Each of the interferometers comprises an at least partly common first optical path leading to an object location, and a respective second optical path for each interferometer, wherein each of the second optical paths leads to a respective reference
10 reflector assembly. At least device is provided for producing an enlargement of the correlation function of the source when placed in at least one of the second optical paths. Scanning means are provided for transversely scanning an optical output from the interferometers over a predetermined area, together with interface optics for transferring an optical beam from the scanning means to an object situated at the object
15 location, and for transferring an optical output beam reflected and scattered from the object back to the interferometers, along the first optical path. Means are provided for directing at least a portion of the returned optical output beam towards the reference reflector assembly, and means are provided to alter at least one of the first optical path and the second optical path, to introduce intensity modulation, phase modulation, or
20 intensity modulation and phase modulation.

In this embodiment, each of the at least two interferometers is excited by an optical source consisting of broadband optical sources or a source having adjustable coherence length in the range of 10 μm to 300 μm . The apparatus further comprises comparator or analyzing means, coupled to the scanning means for comparing a signal
25 representative of the optical beam transferred to the object, with the output signal from the respective reference reflector assembly, so as to demodulate and produce an output from each of the interferometers. Longitudinal scanning means is provided to alter the length of the first optical path or the second optical path in each interferometer simultaneously in steps or continuously, at a pace synchronized with the transversal

scanning means; and means is provided for displaying or storing two images of at least part of the object based on the output signal from each interferometer.

Embodiments of the invention provide:

- a unique OCT system with adjustable depth resolution from the minimum achievable with the largest bandwidth optical source used in the system up to values exceeding the depth resolution of the confocal scanning systems providing sequential or simultaneous images with different depth resolution;
- an apparatus including both an OCT and an optical confocal system which both share the same collecting optics;
- an apparatus including two or more OCTs, each creating independent OCT images with different depth resolution covering a range from the minimum achievable with the largest bandwidth optical source used in the system up to values exceeding the depth resolution of the confocal scanning systems.

For preferred embodiments, the measurements involve non-invasive cross-sectional imaging in biological specimens with one particular application in the eye imaging and more specific for the retina imaging.

BRIEF DESCRIPTION OF THE DRAWINGS:

The novel features which are believed to be characteristic of the present invention, as to its structure, organization, use and method of operation, together with further objectives and advantages thereof, will be better understood from the following drawings in which a presently preferred embodiment of the invention will now be illustrated by way of example. It is expressly understood, however, that the drawings are for the purpose of illustration and description only and are not intended as a definition of the limits of the invention. Embodiments of this invention will now be described by way of example in association with the accompanying drawings in which:

Figure 1A is a diagram of embodiment of an OCT using both optic fiber and bulk components;

Figure 1B is a diagram of embodiment of an OCT using only bulk components;

Figure 2 shows an embodiment of an OCT tomographic mapping apparatus with adjustable depth resolution which is based on the OCT of Figure 1 and which uses a source with adjustable coherence length;

Figures 3, 4, 5, 6, 7 and 8 show alternative sources with adjustable coherence length for use in the present invention;

Figure 9 shows an embodiment of a tomographic mapping apparatus with adjustable depth resolution, which uses a modified version of the source with adjustable coherence length shown in Figure 8;

Figure 9A shows an alternative circuit of the embodiment of Figure 9, employing a computer controlled comparator;

Figure 10 shows a second embodiment of the present invention;

Figure 10A shows an alternative circuit of the embodiment of Figure 10, employing a computer controlled comparator;

Figure 11 shows an optical confocal receiver using a pinhole and lenses, with adjustable focal depth sectioning interval for use in the present invention;

Figure 12 shows a further optical confocal receiver for use in the present invention wherein a fiber is used as aperture in the receiver to ensure a small depth sectioning interval;

Figure 13 shows a third embodiment of the present invention wherein a fiberized coupler is used as the said optical splitter;

Figure 13A shows an alternative circuit of the embodiment of Figure 13, employing a computer controlled comparator;

Figure 14A shows another embodiment of a tomographic mapping apparatus with adjustable depth resolution using both optic fiber and bulk components which can sequentially provide two tomographic images with different sectioning intervals;

Figure 14B shows another embodiment of a tomographic mapping apparatus with adjustable depth resolution using only bulk components which can sequentially provide tomographic images with two different sectioning intervals, and for at least one of the images being possible to adjust the depth resolution;

Figures 14C and 14D show alternative circuits of the embodiments of Figures 14A and 14B, respectively, each employing a computer controlled comparator;

Figure 15 shows a fourth embodiment of an optical coherence tomography mapping apparatus for use in the present invention;

5 Figure 15A shows an alternative circuit of the embodiment of Figure 15, employing a computer controlled comparator;

Figure 16 shows an element to enlarge the correlation function of a broadband source;

10 Figure 17 shows another element to enlarge the correlation function of a broadband source;

Figure 18 shows a further embodiment of the present invention;

Figure 18A shows an alternative circuit of the embodiment of Figure 18, employing a computer controlled comparator;

Figure 19 shows another embodiment of the present invention;

15 Figure 19A shows an alternative circuit of the embodiment of Figure 18, employing a computer controlled comparator;

Figure 20 shows a feedback loop for use in the present invention;

Figure 21 shows a longitudinal scanning device for use in the invention;

20 Figure 22 shows a further longitudinal scanning device for use in the invention; and

Figure 23 shows a further longitudinal scanning device for use in the invention where the incoming direction of the beam is different from its outcome direction.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS:

25 Components which are the same in the various figures have been designated by the same numerals for ease of understanding.

Where optical fibers are used, this is only as an example and it should be noted that a bulk implementation is equally feasible, in which case the respective elements in the examples using fiberized components, are to be replaced by optical paths and
30 the couplers by plate beamsplitters.

A fiber and a bulk implementation of a device 40 for carrying out OCT, are shown in Figures 1A and 1B, respectively, where the source 50 is broadband and coupled to an optical coupler (beamsplitter) 44. The source has a central wavelength suitable for the particular object to be investigated. For eye investigation, a wavelength in the near infrared, such as 800-900 nm, is selected. The broadband source 50 may be for example one or more light emitting diodes, super luminescent diodes, bulb lamps or short-pulse lasers combined to produce the largest possible bandwidth and minimum spectrum ripple by techniques known in the art.

The light received by the coupler (beamsplitter) 44 is split into a first fiber optic path (or free space path) 4 leading to scanning sample assembly 10 which includes means known in the art, as galvanometer scanners, polygon mirrors, resonant scanners, acousto-optic modulators, rotating or vibrating prisms, etc. The scanner head is under the control of triangle, sawtooth or DC voltages produced by a generator 34. The second optic output of coupler (beamsplitter) 44, a fiber (path) 41, leads to a focusing element 75 and to a reference reflecting assembly 46, mounted on a translation stage 48. Other means of altering the reference optical path can be used, in the form of well known optical devices and components; or by using the arrangements shown in Figures 21, 22 or 23, based on galvanometer mirror, lens and mirrors in a suitable arrangement to receive the light from one fiber and send it back to the OCT via a different fiber. The light reflected by the reference assembly 46 is injected into a second coupler (beamsplitter) 42 via an optical focusing element 77, fiber (path) 43, where the coupler (beamsplitter) 42 is tied to the coupler (beamsplitter) 44 via a fiber (path) 5. The outputs of the coupler (beamsplitter) 42 are applied to photodetectors 402 and 404 whose outputs are tied to the inputs of a differential amplifier 45. For a coupler (beamsplitter) 42 with 50% coupling ratio, an ideal balanced detection technique is implemented

The fiber (path) 4 and fiber (path) 5, along with the scanning head 10 and interface optics 12 define an object path, returning the object signal. The scanning head 10 can be divided in two parts separated by optical elements like lenses and/or mirrors in configurations known in the SLO art or general raster scanning systems, in

which case the scanner head 10 and interface optics 12 are interleaved to each other, in one block, and only for convenience they are represented here separately. The fiber (path) 41, assembly 46 and fiber (path) 43 constitute a reference path and are circulated by the reference signal. The object signal interferes with the reference signal in the optical coupler (beam splitter) 42, when the optical path difference (OPD) between the reference path and object path is less than the coherence length of the source 50.

To maximize interference, the polarization in the interferometer is adjusted using polarization controller devices (not shown).

For the bulk version shown in Figure 1B, focusing element 756 is needed for the source 50, focusing elements 757 and 758 are needed for the photodetectors 402 and 404.

In the OCT shown in Figure 1A, the optical fiber of path 43 is wrapped around a piezoelectric crystal transducer or actuator 408 which vibrates in response to the electric signal applied by a sinusoidal generator 410, to produce the phase modulation necessary to facilitate interference detection. However, the phase modulator can be placed anywhere in the reference path or in the object path. Other means of phase modulation can also be used, as fiberized phase modulators, fiber stretchers or bulk crystals, these being used with preference in the bulk version as shown in Figure 1B, as electro-optical, acousto-optical, or magneto-optical modulators, or vibration of the reflecting mirrors in the reference assembly 46.

Alternatively, modulation introduced by the transversal scanner head 10 can be used.

In the present invention, Doppler shift introduced by the reference path is not employed, and the transversal scanning of the object is much faster than the longitudinal scan. When generating a transversal OCT image, the optical path imbalance is advanced after the transversal raster is completed or the path imbalance is varied at such a low speed, that the path imbalance between the point in the object at the beginning of the raster and the point in the object at the end of the raster is less than or only a few times larger than the coherence length of the source.

In addition, if the image size is sufficiently large, there is no need for a supplementary device to introduce phase modulation and the phase modulation created by transversely scanning the object could be the only modulation employed.

The OCT image results as the projection of a sampling function on the target.
5 Due to the target profile, the sampling function varies across the target and consequently the frequency of the signal generated varies. The DC and low frequencies can be eliminated, as they correspond to low transversal definition and by doing so, the low frequency noise is also rejected.

In order to prevent dispersion, which can enlarge the correlation profile,
10 lengths of glass in the object and reference paths should be substantially equal and eventually the remaining dispersion in the glass and dispersion in the object should be compensated by means such as known in the art, using lengths of optical material with suitable index of refraction and dispersive properties placed anywhere in the reference path, as for instance between the elements 75, 77 and the assembly 46, or in the object
15 path in the interface optics 12.

The OCT demodulation block 406 uses a band pass filter on the phase modulator carrier, then a rectifier and low pass filter, or band pass filters tuned on an even and odd multiple of the carrier frequency, followed by individual rectifiers and low pass filters and a summator (not shown), and by a processor, which can produce
20 the linear, the squared, or logarithmic version of the signal amplitude.

Figure 2 shows, in diagrammatic form, a first embodiment of an ophthalmic apparatus 100 in accordance with the present invention. As shown in Figure 2, the apparatus 100 comprises an OCT interferometer 40 excited by a source 500 with adjustable coherence length. The image is displayed and recorded by means of a
25 suitable display device 19, such as a frame grabber, a storage oscilloscope or a suitable printer. The display device 19 is under computer 32 control. Using a coherence length larger than, say 300 μm (the actual depth resolution of commercial SLOs), OCT transversal images with a depth resolution similar to those offered by existing SLO are obtained. Then, by reducing the coherence length, the depth resolution may be
30 improved to determine the thickness of some features in the object volume (the retina).

Various implementations of a source with adjustable coherence length as the source 500 in accordance with various embodiments of the invention are shown in Figures 3 through 8.

One embodiment of a source with adjustable coherence length, which is shown in Figure 3 uses a combination of two sources, one broadband 55 (one or more lamps, SLDs or mode-locked lasers) and the other 57 with a larger coherence length (single mode laser diode or another type of laser with a coherent length larger than the coherence length of the broadband source 55; or a large bandwidth source as, for instance, an SLD, equipped with an optical filter or with a set of optical filters to narrow its line width). The optical powers are added via the electrically controlled directional coupler 62 with a suitable coupling ratio depending on the powers of the two sources, and delivered to the OCT 40, via the fiber 3. The coupler 62 is used to switch and weigh the contribution of each field sent to the OCT 40, under the control of a driving unit 64. Alternatively, a beam splitter can be used instead of the coupler, in which case an index matching gel is not necessary.

In order to cover the entire scene of an image over 40° which is usually the angle field used in SLO, at least 300 μm coherence length will be necessary, taking into account a medium curvature of the wavefront at the back of an eye lens of focal length 2 cm, and the heights of optical nerve layers. The two sources in Figure 3 have the same central wavelength and the coherence length of the coherent source 57 must be restricted to prevent matching of a fiber end reflection, (when the interferometer in the OCT 40 is in fiber, or any other reflection from the faces of optical bulk elements when the interferometer is in bulk) with features inside the investigation volume. The coherence length of the source 500 is adjustable under the control of the electric field applied to the coupler 62. Weighting the powers delivered by the two optic sources 55 and 57, the equivalent coherence length of the overall optic field injected into the system is adjustable. In fact, two images are created, one with a narrow sectioning depth due to the source 55 and the other with a larger sectioning depth due to the source 57. Reducing the power of the first and increasing the power of the second, has

the effect of bringing into view features from background of the image created with the broadband source.

Typically, the coherence length of the first source 55 may be less than $100\mu\text{m}$, and may be adjustable in the range of $10\mu\text{m}$ up to $300\mu\text{m}$.

5 In the present disclosure, a cumulating OCT image produced by both sources is displayed without recurring to longitudinal mirror shift, and a unique bandpass filter for the signals produced by both sources is used to pass the bandwidth due to the phase modulation introduced by transversely scanning the object or tuned on the phase modulation frequency introduced by an external phase modulator.

10 Figure 4 shows a second embodiment of a source with adjustable coherence length 500, where a micrometer translation stage 82 is employed to shift and position the collecting fiber 3, input to the OCT system 40, in such a way to collect signals of different strengths from the output of the sources 55 and 57 via the fibers 71 and 73, respectively.

15 Figure 5 illustrates an alternative embodiment of a source 500, where a micrometer translation stage 82 is employed to shift and position the collecting fiber 3, input to the OCT system 40, in such a way to collect signals of different strengths from the output of the sources 55 and 57, suitably orientated and equipped with micro optics elements to ensure a sufficient coupling of either source into fiber 3.
20 Equivalently, when the two sources 55 and 57 are arranged in a line parallel to the direction of movement of the stage 82, the fiber 3 can be replaced with a mirror oriented at 45° to the direction of movement of the translation stage 82, which when moved in the direction shown by the double arrow, intercepts all or parts of the output beams of the two sources.

25 Figure 6 details yet another embodiment of the source 500, where a special optical source, 92, with electrically adjustable coherence is used (for instance, a multi-electrode laser diode, which, depending on the driving conditions of different electrodes, can supply a very coherent field or can deliver an incoherent field to the OCT 40). Such multi-electrode laser diodes can behave as an SLD (broadband source)
30 or as a very coherent laser source. The driver 94 ensures a suitable set of currents or

control voltages pass through the control pins of the source 92, to vary the coherence length. The source spectrum may have small satellite coherent peaks. If such extra peaks exist, they must appear at distances greater than the operational range of the system. For the retinal applications, 2 mm is a minimum and usually the solid state
5 lasers have 1 mm width cavities which give repetition of correlation peaks at 2 mm. Laser sources with cavity lengths of greater than 2 mm can also be used.

Another embodiment of a source with adjustable coherence length 500 is shown in Figure 7, where a tunable source 96, is tuned at a rate faster than the bandwidth of the processing receiver in the OCT. Such rate may be in the nanosecond
10 or subnanosecond range. One version for the tunable source 96 uses a multi-electrode laser diode or a DFB laser. The principle involved in this case is that of a source with synthesized coherence. The driving electronics 98 are capable of applying very fast pulses to enlarge the source spectrum at the level necessary for a good OCT sectioning capability. Equivalent coherence lengths of 300 μ m to a few meters are obtained in
15 this way. The depth resolution of the apparatus is adjustable by changing the amplitude of modulation pulses applied.

Figure 8 shows another embodiment of a source with adjustable coherence length 500, where the two sources 55 and 57 are added via the directional coupler 58 with a suitable coupling ratio depending on the powers of the two sources, and
20 delivered to the OCT 40, via the fiber 3. Alternatively, a beamsplitter can be used instead of the coupler 58 in which case 3 represents the optical output, and the index matching gel 59 is not necessary. The coherence length of the source 500 is adjustable under the control of knob 51. The power dependence of the optical sources on the control parameter, adjusted via the drivers 54 and 56 of the respective optical sources,
25 may be linear or nonlinear; for instance the SLD power dependence is more or less linear with the injecting current, while the laser diode dependence is very nonlinear. The same is true for the FWHM spectrum of a laser diode as an example of coherent source which can be used as source 57. The control electronics 52 ensures that a smooth dependence, preferably linear (or as deemed suitable for the applications or
30 clinical use), is implemented across the range of rotation angle of the knob 51, and the

range of depth sectioning interval is adjusted in this way. The control electronics ensures also that for each position of the knob 51, the power at the output 3 is constant and does not exceed the safety value on the retina for ophthalmic applications. For such applications, the coherence length should be adjustable from the minimum
5 ensured by the broadband source 55 up to at least 300 micrometers. Alternatively, one or both of the sources 55 and 57 in Figures 3, 4, 5, and 8 could be of the type presented in Figure 6 and 7.

Figure 9 diagrammatically shows an ophthalmic instrument according to the invention where the two images created by each of the sources used in Figures 8 are
10 displayed simultaneously. To this end, the two sources in the said source with adjustable coherence length are modulated in intensity at two different frequencies, using the generators 651 and 652; and two band pass filters, 101 and 102 tuned on these two different frequencies are used to separate the signals, with the necessary image bandwidth.

15 The signals delivered by the two bandpass filters, are weighted by the potentiometers 27 and 29, respectively, at the inputs of a summator 24, the resultant signal being displayed and recorded by means of a suitable display device 19, such as a frame grabber, a storage oscilloscope or a suitable printer. The two signals are also applied to the device 19, which can display one or both of these signals, or the
20 weighted combination under the computer 32 control.

Alternatively, as shown in Figure 9A, a comparator 135 can be used in place of summator 24 and potentiometers 27 and 29, under the control of software in the computer 32 over control line 137, to deliver a weighted signal to the display device 19. The two signals from the bandpass filters 101 and 102 are also delivered to the
25 display device 19, as before.

In fact, the comparator 135 may be such that it will operate digitally, in that it may be a multiplying digital to analog convertor, taking analog signals from the bandpass filters 101 and 102 and under the control of a signal input from the computer 32, manipulating the signals in a manner whereby a weighted signal is produced under
30 by manipulative control by the computer 32 so as to adjust for or modulate a weighted

signal having regard to the intensity of the signal coming from the two bandpass filters 101 and 102. An analog signal is then output to the display device 19.

Alternatively, an analog multiplier can be employed, under the control of the computer 32, within the comparator 135; once again, giving an analog output which is applied to the display device 19.

Indeed, the following discussion with respect to the comparator or analyzing means is relevant to all embodiments described herein, where a comparator 135 is referred to.

The comparator or analyzing means includes two inputs for analog signals which are applied thereto, and one analog output signal. It also includes an input for receiving control signals from the computer. There is at least one analog to digital convertor for converting at least one of the two analog signals which are input to the comparator or analyzing means, for digital manipulation under the control of the computer so as to produce a weighted output signal. The comparator or analyzing means also includes a comparator for comparing a weighted output signal from the at least one analog to digital convertor to a signal which is representative of the other of the two analog input signals, so as to produce an output analog signal from the comparator or analyzing means which is a function of the at least weighted output signal and the signal representative of the other of the two analog input signals.

Alternatively, the comparator or analyzing means may include a multiplying digital to analog convertor which is capable of receiving the two analog input signals and outputting the one analog output signal under the control of the computer. In this case, each analog input signal is converted to a digital signal, and at least one of the resultant digital signals is multiplied by a weighting factor under the control of the computer. The product signals are added, and then converted to an analog signal so as to produce the analog output signal.

Yet another alternative provides for the comparator or analyzing means to include at least one analog multiplier which functions under the control of the computer acting on at least one of the two input analog signals so as to produce a multiplier product signal having a value in the range of $1/n$ to $n-1/n$ times the original

input analog signal being acted upon. N is typically a whole integer which ranges from 2 to 256. A comparator means is provided for comparing the multiplier product signal to a signal representative of the other of the two analog input signals so as to produce an output analog signal from the comparator or analyzing means which is a function of the at least one weighted output signal and the signal representative of the other of the two analog input signals.

Figure 10 diagrammatically shows an ophthalmic instrument according to a second embodiment of the present invention. As shown in Figure 10, the apparatus 100 comprises an OCT interferometer 40 excited by a source which can be either broadband, 50, or with adjustable coherence length, 500. In each of Figures 2 and 10, an OCT sample beam 4 is output from OCT interferometer 40, in fiber if the OCT interferometer is in fiber, or if it is in bulk, 4 is an optical output beam. The OCT sample beam output 4 is focused by an optical element 6, such as a refractive or reflective optical element, split by a beamsplitter 8 into a beam 9 which is then deflected by a 2D scanner head 10 to scan transversely, via interface optics 12, to an object 13. In Figure 10 the object 13 is an eye, the beam being focused by the eye lens 15 onto the retina 17. The light returned by the object, reflected and scattered, is partly collected via the focusing element 6 back into the path 4 and partly, a beam 11, collected by a confocal optical receiver (COR) 20. The signal delivered by the OCT, 23, and the signal delivered by COR at its output 21 are weighted by the potentiometers 27 and 29 respectively at the inputs of a summator 24, the resultant signal being displayed and recorded by means of a suitable display device 19, such as a frame grabber, a storage oscilloscope or a suitable printer. The device 19 is under computer 32 control. The signals of the OCT and COR are also applied to the device 19, which can display one or both of these signals under the computer 32 control. The images can be displayed in linear or logarithmic scale on grey or false color coded format. When the OCT and COR images are to be displayed separately, a special device 19 with dual display capabilities is required.

Just as in the embodiment of Figure 9, a comparator 135 can be used as shown in Figure 10A to compare the signals 21 and 23, under the control of the computer 32 over control line 137, to deliver a weighted signal to the display device 19.

Figure 11 diagrammatically shows an embodiment of the confocal optical receiver 20 for the embodiment of the invention in Figure 9, equipped with the lenses 22 and 26, a pinhole 25 being placed in the focal plane of the lenses 22 and 26, with the lens 26 removed when simpler implementation is acceptable. After passing through the lenses 22, 26, the light is collected by a photodetector 28. The photodetected current is amplified in an amplifier 30 and supplied to the input 21 of the display device 19. By modifying the pinhole 25, or the focal lengths of the lenses 22 and 26 and their distances to the pinhole 25, different depth sectioning intervals are obtained. A resolution of 300 μm is available for the COR when the object is the eye, in which case the confocal receiver 20, the splitter 8 along with the scanner head 10 and the interface optics 12 act as an SLO. When the aperture 25 is open at maximum, the image will look contiguous, not fragmented, and the entire scene will occupy the display, with pixel-to-pixel correspondence with the OCT image. Consequently, when the embodiment of Figure 10 is equipped with the confocal receiver of Figure 11, three possibilities to adjust the depth sectioning interval exist. The first possibility consists in adjusting the depth sectioning interval of the COR image by means of devices in the COR which are independent of the source used, either broadband 50 or adjustable coherence length 500. Such adjustment provides a depth sectioning interval adjustable from 300 μm upwards when the object 13 is the eye. A second possibility consists in varying the sectioning interval of the OCT image by changing the coherence length of the source 500; in this case, the depth sectioning interval on the OCT image can be adjusted from the minimum given by the minimum coherence length of the source 500, say 10 μm , up to the maximum coherence length of the source 500, say 300 μm , providing an adjustment interval on the OCT image which is complementary to the interval provided by the COR image. A third possibility consists in weighting the OCT and COR signals applied to the input of the summator 24 in Figure 10, by means of potentiometers 27 and 29 when the optical source is broadband, 50. If the source

used is the source with adjustable coherence length 500, a more diverse adjustment can be operated, actuating on both the sectioning interval of the OCT image and on the weighting of the OCT and COR signals.

Figure 12 diagrammatically shows another embodiment of an optical confocal receiver 20 for use in the embodiment of the invention of Figure 9, where the aperture of a multi-mode or single-mode fiber 31, pigtailed to a photodetector 28, is used to ensure a high confocal condition. In this case, the depth sectioning interval on the image displayed using the signal from the confocal optical receiver, COR, is not adjustable. For this embodiment, the sectioning depth interval in the final image can be adjusted only by weighting the OCT and COR signals applied to the input of the summator 24 in Figure 10, by means of potentiometers 27 and 29 when a broadband source 50 is used. When the source with adjustable coherence length 500 is used, two procedures for adjusting the depth sectioning interval are possible: weighting the OCT and COR signals, or adjusting the OCT depth sectioning interval by changing the coherence length of the source.

Figure 13 diagrammatically shows a third embodiment of the present invention, where the beamsplitter 8 is now replaced by a directional coupler 800 and the light returned from the object path, i.e.: from the object 13, via the interface optics 12, the scanner head 10 and focusing element 6 is sent to the confocal receiver 20 via the fiber 2 and fiber 11, the signal from the confocal optical receiver, COR, being obtained after photodetection in the pigtailed photodetector 28 and amplification by amplifier 30. Preferably, the fiber ends 2 and 16 are angle-cut and the fiber end 16 is placed in index matching gel 59 to reduce the amount of light from the OCT source being reflected towards the confocal receiver. For this embodiment, the depth sectioning interval on the image displayed using the signal COR is given by the numerical aperture of the fiber 2 and is not adjustable. The sectioning depth interval in the final image can be adjusted only by weighting the OCT and COR signals applied to the input of the summator 24, by means of potentiometers 27 and 29 when a broadband source 50 is used. When the source with adjustable coherence length 500 is used, two procedures for adjusting the depth sectioning interval are possible: weighting the OCT and COR

signals or adjusting the OCT depth sectioning interval by changing the coherence length of the source.

Once again, as described above, a comparator can be used as shown in Figure 13A, under the control of the computer 32 over control line 137, to compare the signals 21 and 23, and to deliver a weighted signal to the display device 19.

Figure 14A shows, in diagrammatic form, a fourth embodiment of an (ophthalmic) apparatus 100 in accordance with the present invention, which can sequentially display two images of very different depth resolution. As shown in Figure 14A, the apparatus 100 comprises a fiberized interferometer 40. Two regimes of operation are selectable: OCT and confocal by means of a switch, 603, which for the confocal regime, synchronously shifts an opaque screen, 605, into the reference beam of the interferometer, and larger amplification of the photodetected signal in the differential amplifier 604 is applied before being displayed by display device 19, such as a frame grabber, a storage oscilloscope or a suitable printer. When balance detection is used, the differential amplifier 604 has also the function of addition of the two photodetector signals instead of being subtracted as for the OCT regime. The display device 19 is under computer 32 control. In the confocal case, the fiber aperture acts as a confocal restricting aperture, which depending on the fiber used, determines a depth sectioning interval of 0.5-2 mm.

If the photodetectors 402 and 404 are avalanche, the photodetection gain is switched between a large value obtained in the regime of multiplication for the confocal case and a small value in the OCT case when the avalanche photodetectors have little or no multiplication, by simply blocking or unblocking the reference power, the consequent voltage drop on the resistor in series with the avalanche photodetector when large optical power is applied acting as a gain control.

In either case, depending on the position of switch 603, either the differential amplifier 45 and demodulator 406, or the amplifier 604, can be replaced by a comparator under the control of the computer 32, to deliver a weighted signal to the display device 19.

Figure 14B shows, in diagrammatic form, another embodiment of an (ophthalmic) apparatus 100 in accordance with the present invention, which can sequentially display two images of very different depth resolution, one image admitting adjustment of the depth resolution. As shown in Figure 14B, the apparatus 100 comprises a bulk interferometer 40, equipped with synchronous adjustable pinholes 762 and 764 or synchronous adjustable focusing elements 757 and 758 to alter the numerical aperture of the receiving photodetectors 402 and 404. Two regimes of operation are selectable: OCT and confocal by means of a switch 603, which for the confocal regime, synchronously shifts an opaque screen, 605 into the reference beam, and larger amplification of the photodetected signal in the amplifier 604 is applied before the being displayed by display device 19, such as a frame grabber, a storage oscilloscope or a suitable printer. When balance detection is used, as shown in Figure 14B, the amplifier 604 has also the function of adding the two photodetector signals instead of being subtracted as for the OCT regime. The display device 19 is under computer 32 control. In the confocal case, the depth resolution is adjustable by varying simultaneously the numerical apertures of the two collecting optics, either the pinholes 762, 764 or focusing elements 757 and 758, which when imaging the eye, could cover a range, from 300 μm upwards. Obviously, in Figures 14A and 14B, the depth resolution can be made adjustable by means of the source 500 with adjustable coherence length, as described above.

In the case of the embodiment of Figure 14B, just as above in the case of the embodiment of Figure 14A, depending on the position of switch 603, either the differential amplifier 45 and demodulator 406, or the amplifier 604, can be replaced by a comparator 135 under the control of the computer 32 over control line 137, to deliver a weighted signal to the display device 19.

Figures 14C and 14D show alternative circuits of the embodiments of Figures 14A and 14B, respectively. In each of these cases, the analog output signals from photodetectors 402 and 404 may be converted in the comparator 135 to a digital signal so that a weighted output signal can be applied to the display device 19. Again, typically a multiplying digital to analog convertor for each signal may be employed,

where the multiplication factor is determined under the control of the computer 32, or an analog multiplier under the control of the computer may be employed within the comparator 135. For example, adjustments can be made over a range of $1/256$ up to $255/256$ in respect of the weight of the signal from either photodetector 402 or 404, with respect to the comparison and weighting of the signal from the other photodetector 402 or 404.

Figure 15 diagrammatically shows a fifth embodiment of an optical mapping apparatus with adjustable depth resolution, where an optical element 112 is introduced in the object or reference path of the OCT interferometer 40, with the effect of enlarging the correlation profile of the source. In Figure 15, the same phenomenon of dispersion is used effectively to increase the size of the fragments sampled by the OCT from the target, this increase is due to an equivalent enlargement of the correlation function of the broadband optical source when measured with an interferometer with an OPD about zero. The element 112 acts as an OPD spread enlarger. This element is a dispersive element, a diffractive element, or a special device, as shown in Figure 16 and Figure 17, respectively. A dispersive element is used to increase dispersion controllably, to such an extent as to increase the depth sectioning interval of the instrument over $100\text{ }\mu\text{m}$. The OPD spread enlarger 112 is based on known variable dispersion means. The higher the dispersion, the higher the enlargement of the coherence length. An enlargement of up to $300\text{ }\mu\text{m}$ is possible using high dispersion materials, as for instance 2.07 mm ZnSe increases the coherence length of a laser TiAl_2O_3 from $2.1\text{ }\mu\text{m}$ to $268\text{ }\mu\text{m}$.

Once again, as shown in Figure 15A, and as described above, the differential amplifier 45 and demodulator 406 can be replaced by a comparator 135 so as to deliver a weighted signal 23.

The OPD spread enlarger element described in Figure 16 uses two prisms 122 and 124 of convenient width and index of refraction. Adjusting the length of path in glass, the depth sectioning interval of the instrument 100 can be adjusted. This element can be placed in either the object or the reference path. In Figure 15, the

element 112 is placed in the reference path between the fiber 41 and the reference assembly 46. If the OCT interferometer 40 is in bulk, the lens 75 can be removed.

The OPD spread enlarger element shown in Figure 17, uses a number of very thin parallel glass plates, (nine are shown in Figure 17), between two lenses 75 and 136. The element in Figure 17 can also be implemented by means of integrated optics. Using two lenses as shown, such a system can be placed in a section of fiber. For bulk interferometer implementation of the OCT 40, the lenses 75 and 136 can be removed. The device shown in Figure 17 provides 9 different beams with increasing optical paths, spreading the OPD profile of the source correlation function. The power of each delayed beam is proportional with the integral of the power distribution in the beam over the area of the respective plate. In order to ensure that all 9 beams have the same power, the width sampled by the beam out of each plate is weighted with an inverse proportional law to the power distribution within the cross sectional area of the beam. By designing the width of each plate intercepting the beam in relation with the position of the plate in the enlarged beam between the lenses 75 and 136 in Figure 17, an overall Gaussian profile for the correlation function can be obtained, which can simulate the resolution profile in depth of an SLO with the same equivalent depth width.

Figure 18 diagrammatically shows a sixth embodiment of optical apparatus for mapping objects with adjustable depth resolution 100 according to the present invention. The apparatus 100 comprises a different OCT, where 2 interferometers are shown for simplicity. More interferometers could be installed, if desired. The fiber path 5 is split into two and two more couplers 434 and 422 are introduced. The object path of the first interferometer is via the fiber 33, coupler 434, fiber 5, coupler 44 to the fiber 4, scanner 10 and object 13 and then returns back via the same elements to the coupler 42. The reference path is via the coupler 44, element 75, assembly 46, element 77, fiber 43 and coupler 42 with the interference signal processed by the photodetectors 402 and 404. The second interferometer has its object path via the fiber 35, coupler 434, and then shares the same elements with the first interferometer object path. The reference path of the second interferometer uses the reflector 454 and the

beamsplitter 452, supported by the assembly 432 which is mounted along with the assembly 46 on the same device 48 for longitudinal scanning, the OPD enlarger 112, beam 45, and the interference signal is processed by the photodetectors 424 and 426. Alternatively, the two reference paths can be simultaneously scanned using a fiber wrapped around piezo-cylinder placed in the common path of both reference paths, i.e., along the fiber 43, in which case the position of elements 46 and 432 are adjusted to equalize the reference paths, and the device 48 is removed. Any other device for longitudinal scanning such as described in relation to the OCT in Figure 1, can be used. The OPD spread enlarger 112 can be implemented using either of those shown in Figures 16 or 17, or using a diffractive element. The two reference paths, one including the fiber 41, assembly 46, fiber 43 and the other including fiber 41, beamsplitter 452, mirror 454, OPD spread enlarger 112 and air path 109 are substantially equal, when the lengths of the fibers 33 and 35 connecting the coupler 434 to the couplers 42 and 422 are also equal. Any substantial differences in the fiber lengths of the coupler 434 can be compensated for in either of the paths 41, 43 or 45 in order to ensure coherence matching and keeping dispersion low in the first interferometer. On the other hand, it would be desirable to have the air path 109 short, to help with the dispersion in the second interferometer. The demodulator 406 processes the signal from the first interferometer, which provides the image with the best depth resolution out of all the other interferometers, and drives the input 23 of the display device 19, while the demodulator 428 processes the signal with the larger sectioning interval provided by the second interferometer, and drives the input 21 of the display device 19. Practically, this embodiment of the optical mapping apparatus with adjustable depth resolution replaces the COR channel in the embodiment in Figure 10 with an OCT channel of similar depth resolution, as obtained in the second interferometer in Figure 18. The display device 19 is equipped with means to display the two images separately or/and to display pixel-by-pixel a combination of the two images in a single image.

The schematic diagram in Figure 18 can be extended to include more interferometers, for instance by extending the coupler 434 from 1:2 to 1:n, and

devising a bulk equivalent splitter for the assemblies 432 and 46 to divide the reference beam output of fiber 41 into n reference beams, with all the reference paths adjusted simultaneously by shifting the translation stage 48 and with $n-1$ interferometers, containing different OPD enlarger elements, creating corresponding images with different depth sectioning widths.

In any event, as shown in Figure 18A, and as described above, a comparator 135 can be used in place of the summator 24 and potentiometers 27 and 29, under the control of software in the computer 32 over control line 137, to deliver a weighted signal to the display device 19. The signals from the demodulators 406 and 428 are also delivered to the display device 19, as before.

Figure 19 diagrammatically shows a seventh embodiment of an optical apparatus for mapping objects with adjustable depth resolution 100 in accordance with the present invention. The apparatus 100 comprises a different OCT where two interferometers are shown for simplicity. More interferometers could be installed if desired with the requirement that the two (or all the) interferometers have the same object path. The object path is via the fiber 5, coupler 44 to the fiber 4, scanner 10 and object 13 and then returns back via the same elements to the coupler 42. The two reference paths have in common the fiber 41, element 75, assembly 46, and the beamsplitter 452 and the output fiber 63 of the coupler 435. After the beamsplitter 452, supported by the assembly 432, the nondispersive reference path continues via element 77, fiber 43, phase modulator 408 to coupler 435, with the cumulated glass length substantially equal with the glass length in the object path. The second reference path, which is dispersive, continues via the OPD spread enlarger 112, mirror 454 supported by the assembly 432, phase modulator 425, element 78 and fiber 65 to the coupler 435. The phase modulator 425 is driven by the sinusoidal generator 409 at a frequency f_2 , much larger than f_1 + double the image bandwidth, where f_1 is the frequency of the sinusoidal generator 410 driving the modulator 408 in the nondispersive reference path. The phase modulator 425 uses an electro-optic, or an acousto-optic or a magneto-optic modulator, or a fiberized modulator which is mounted on the fiber 65. Similarly, the phase modulator 408, can be equally

implemented in bulk using an electro-optic, acousto-optic or a magneto-optic modulator, in which case it is mounted between the beamsplitter 452 and the element 77. The assembly 432 is mounted along with the assembly 46 on the same device 48 for longitudinal scanning. Alternatively, the two reference paths can be simultaneously scanned using a fiber wrapped around piezo-cylinder placed in the common path of both reference paths, i.e.: along the fiber 41 or 63, in which case the position of elements 46 and 432 are adjusted to equalize the reference paths, and device 48 is removed. Any other device for longitudinal scanning such as described in relation to the OCT in Figure 1 can be used. The OPD spread enlarger 112 can be implemented using either of the embodiments shown in Figures 16 or 17 or using a diffractive element. The other fiber end of the coupler 435 is terminated in the index matching gel 59 to avoid reflection from it. The two reference optical paths are substantially equal. Any substantial differences in the fiber lengths of the coupler 435 can be compensated for in the paths 41 in order to ensure coherence matching and minimizing dispersion in the nondispersive interferometer. On the other hand, it would be desirable to have 41 and 43 short and 65 longer, to help with the dispersion in the second (dispersive) interferometer.

The signal due to the interference along the first reference path is filtered by the bandpass filter 101 tuned on the frequency f_1 or its multiples. The signal due to the interference along the second reference path is filtered by the bandpass filter 102 tuned on the frequency f_2 or its multiples. The demodulator 406 processes the signal from the first interferometer, which provides the image with the best depth resolution out of the two interferometers, and drives the input 23 of the display device 19. The demodulator 428 processes the signal with the larger sectioning interval provided by the dispersive interferometer, and drives the input 21 of the display device 19. Practically, this embodiment of the optical mapping apparatus with adjustable depth resolution replaces the COR channel in the embodiment in Figure 10 with an OCT channel of similar depth resolution, as obtained in the dispersive interferometer in Figure 19. The display device 19 is equipped with means to display the two images separately or/and to display pixel by pixel a combination of the two images in a single

image. This embodiment has the advantage that it does not divide the object signal prior to the receiving coupler 42, as the coupler 434 does in Figure 18.

The schematic diagram in Figure 19 can be extended to include more interferometers, for instance by extending the coupler 435 from a 1:2 to a 1:n coupler, and devising a bulk equivalent splitter for the assemblies 432 and 46 to divide the reference beam output of fiber 41 into n reference beams, with all the reference paths adjusted simultaneously by shifting the translation stage 48 and with each interferometer containing a phase modulator and a different OPD enlarger element to create each an image with a different depth sectioning width.

As before, and as shown in Figure 19A, a comparator 135 can be used to compare the signals 21 and 23, under the control of the computer 32 over signal line 137, to deliver a weighted signal to the display device 19. In this case, the signals 21 and 23 are also delivered to the display device 19. Of course, care must be taken that the software control from computer 32 is such that the proper weighting factors are applied to the signals 21 and 23 as they are applied to the comparator 135, having regard to the intensities of the analog signal devices from the two bandpass filters 101 and 102.

Figure 20 shows an embodiment of another aspect of the invention. This embodiment permits the planarization or bending of the wavefront at the back of the eye lens. This is obtained by a synchronous control of the OPD in the OCT interferometer in any of the implementations above as shown in Figure 1, Figure 2, Figure 10, Figure 14A, Figure 14B, Figure 15, Figure 18, or Figure 19, by means of feedback directed by the raster scanning means. For each direction towards which the beam is pointed, the controlling feedback block 90 applies a control signal onto an optical delay element 86 in the reference or object path of the OCT. The larger the angle at which the ray enters the eye, the larger the object path length. Each direction is given by two voltages applied by the generator 34 to the transversal scanner 10. The two blocks 84 sense the level of these voltages and output a commensurate voltage. The adder 85 provides the control signal to the optical delay device 86, which could be a sufficient long fiber wrapped around piezo-cylinders. Equivalently, the device 86

can be built using vibrators, as for instance two loudspeakers can shift the two mirror parts of the reflecting element 46 in Figure 1 and Figures 9, 14A, 14B, or 15, along directions at 45° in relation to the axes of the elements 75 and 77. The device 86 can also be built using a galvanometer scanner in association with a grating. Another possibility is to use a galvanometer scanner in association with lenses and mirrors as shown in the present invention in Figure 21 and 22, or two galvanometer scanners in association with lenses as shown in Figure 23. The device 86, depending on implementation, can be interleaved in any of the fibers 4, 5, 41, or 43 in Figure 1A, Figure 14A, Figure 15 or in the fiber paths 4, 5, and 41 only in Figure 18 or in the fiber 5, 41, and 63 only in Figure 19, or in the path 4, 9, 41, or 43 in Figure 1B, Figure 14B or in the equivalent path of the fiber paths when the configurations in Figure 18 and 19 are translated in bulk. The device 86 works at twice the line frequency value, so at twice the frequency of the sawtooth signal applied to the transversal scanner which gives the line in the final image raster. Typically, this means about 1 kHz. The amplitude of the path change introduced by the device 86 should be at least a few hundred microns. The wavefront curvature could be under-corrected, corrected or overcorrected modifying the gain of the summator 85 via the knob 87. For a good correction, i.e.: when the wavefront is plane, the focal length of the eye lens should be known.

Alternatively, the two sensor level elements 84 can be electrical circuits with memories programmed to output a certain voltage for a given input level.

Figure 21 shows an embodiment of a longitudinal scanning means which uses a galvo-scanner to create a fast and low dispersive variation of the optical path. The configuration of 50:50 couplers 544 and 542 is used to implement balance detection. The channel supplied by the photodetector 402 needs twice as much gain as the channel supplied by the photodetector 404.

Consideration will now be given to the case when the interferometer is matched, i.e.: the $OPD = 0$ and the reference beam 155 falls on a point on the galvanometer-mirror 150 away by a quantity δ from the axis of rotation, when the galvo-scanner 152 is moved to the lens 154 by the same quantity (equivalent results

are obtained if the beam falls on the galvo-scanner 152 at $-\delta$). The rays are deflected by the galvanometer-mirror 150, refracted by the lens 154, reflected by the mirror 156 perpendicularly oriented to the optical axis in the focal plane of lens 154, refracted by the lens 154 again and retraced along the original path back to the beam 155 and to the fiber 151 via the focusing element 153. For small scanning angles β , due to a rotation of the $\beta/2$ of the galvanometer-mirror, the path imbalance P introduced between the central ray (along the optic axis) and the ray deflected by an angle β from the optic axis after being reflected from the mirror 154 is given by equation:

$$P = 2\delta\beta \quad (1)$$

For each variation of P by λ , a period of the photodetected beating signal results due to scanning the mirror 156. The frequency of this signal for a triangular driving signal is given approximately by:

$$\nu = \frac{8kF_zV_z}{\lambda}\delta \quad (2)$$

where k is the scanner sensitivity, V_z the amplitude and F_z the frequency of the triangular wave applied to scanner 152. For a ramp signal, the equation (2) should be divided by 2.

In Figure 21, the shift δ was obtained by placing the galvo-scanner 152 closer to the lens 154, in which case the point of incidence, B , of the beam on the galvanometer-mirror is shifted towards the collimator 153, to a point B' , by the same amount. The apparent point, B'' , origin of the fan of the rays deflected is situated on the axis of the lens 154. (If the scanner 152 is moved away from the lens 154, B'' moves in the same direction by about the same distance).

To ensure a telecentric set-up, the distance lens 154 to the mirror 156 and to the point B'' is equal with the focal length of the lens 154.

In this way, the direction of the returned beam is brought parallel to the direction of emergent beam 155 from the lens 153. This arrangement minimizes the parasitic intensity modulation owing to the variation in the light re-injected into the fiber while 150 is driven.

A second embodiment of a low dispersion device for longitudinal fast path variation is shown in Figure 22. In this case the beam 155 falls in the point B , on the

axis of rotation of the mirror 150. The path imbalance variation is created by shifting the lens 154 laterally from the optical axis crossing the point B, by a quantity δ . After crossing the lens 154, the beam is reflected from the mirror 156 in the points a (β _ray), b (0 ray) and c ($-\beta$ ray) and returns to a parallel direction to the incident beam 155 and is incident on a second mirror 157 in the respective points a1, b1 and c1. After the reflection on the galvanometer-mirror 150, it goes back to the lens 154, mirror 156, point B on the galvanometer-mirror 150 and finally along the incident beam 155 back to the fiber 151. For simplicity, the drawing in Figure 22 corresponds to the case when the angle β has such a value that the point b coincides with the axis of the lens 154.

A third embodiment of a low dispersion device for longitudinal fast path variation is shown in Figure 23, which uses two systems in Figure 21 in order to redirect the deflected light to a different fiber (path), useful for the OCTs with balance detection and recirculation of the reference power.

Any of the OCT systems described so far can be used to build longitudinal OCT images. In this case, the transversal scanning system 10 is operated along one direction, X or Y, or is controlled to sample an inclined line, or a circular or elliptical shape. After each such transversal complete cycle, the reference path is stepped or during each such transversal complete cycle the reference path is changed at much smaller speed than the transversal scanning speed, using any devices known in the art to alter the path, or one of the embodiments in Figures 21, 22, or 23. A 2D map is obtained, with one coordinate the depth, explored using the systems for longitudinal scanning and the other transversal, given by the transversal scanner head.

For the embodiments in Figures 21 and 23, when used to produce longitudinal OCT images, the regime of operation of the vertical display of the device 19 in Figures 2, 9, 10, 13, 14A, 14B, 18 and 19 is controlled by the slope of the ramp signal driving the galvo-scanner 152. At every change in the above mentioned slope, the sense of the raster scan in the final displayed frame along the depth direction is changed, i.e.: the voltage applied to the vertical or horizontal plates of the CRT has a triangular shape as different from the sawtooth shape commonly used in TVs and PCs CRTs.

Alternatively, the operation of changing the order of display and of storing can also be implemented electronically in digital format in the display device (frame grabber for instance). In this way, irrespective of the sense of longitudinal scan, the depth axis sense of the image displayed does not change during the longitudinal scan.

- 5 The equations (1) and (2) are equally applicable for galvanometer scanners used for the transversal scanning in OCT systems. In this case, equation (2) gives the frequency of the phase modulation, resulting from scanning a plane target. This "carrier" frequency can be used to carry the image bandwidth with no extra device acting as a phase modulator. The larger the δ , the higher the frequency of the carrier.
- 10 In this way, the more the beam is shifted away from the galvanometer mirror, the larger the bandwidth of the signal which can be carried by the carrier.

- This carrier appears from scanning the optical beam at coherence over the sampling function in the shape of a grid projected over the target. However, any tilts of the target will result in disturbing the value of the carrier. In other words, the
- 15 sampling function is not constant over the target, i.e.: the transversal pixel size varies across the target.

- Consequently, when the phase modulation due to the transversal scanner is employed, the band pass filter of the demodulation block has to allow for the variation of the carrier frequency due to the object tilts, roughness and profile. This is also valid
- 20 when the optical beam is centered on the galvanometer mirror. In this case, as the sampling function looks in the form of Newton rings, the features in the center of the rings will be sampled with a large periodicity, giving rise to carrier frequencies of low frequencies. If the bandwidth used skips 0Hz and some of the low frequency components (in order to reject the 1/f noise), this would mean that the target parts not
- 25 well sampled will be missed in the final image. For this reason, a combination of the modulation introduced by the galvanometer scanner when the beam is centered and the modulation introduced by a phase modulator should be employed. The frequency of the signal driving the phase modulator should be placed in the middle of the spectrum generated by the OCT when scanning the object transversely. Such a combination
- 30 should also be employed when the size of the image is too small (for the human retina,

this means about 0.5 mm transversal), in which case the carrier frequency is less than the bandwidth to be processed.

The transversal OCT images collected at different depths can be software processed to produce an equivalent transversal image, which can take the appearance of a superposed OCT images, or the appearance of the SLO image or of an image
5 sampled out from the volume of the target using a conveniently shaped depth profile.

After collecting N images for N-values of the path imbalance between the first and the second paths in the said interferometers, such an O_s image can be obtained via the equation:

$$O_s(z) = \sum_{p=1}^n [O_{OCT}]_p^n C_p$$

10

(3)

The power $n=1$ and all the coefficients $C_p=1$ means simple superposition. The power $n=2$ means that an equivalent confocal image can be obtained when the coefficients C follows the depth sectioning profile of a confocal microscope. For
15 instance, an image equivalent with the image produced by a state of the art SLO can be generated by using as coefficients C sampled values of its experimental depth sectioning profile.

An immediate advantage follows, such software generated profile will not have the adjacent satellite peaks characterizing the experimental profiles.

20 Other equivalent images can be generated for larger values n .

Using a block which produces the squared version of the coherence signal, i.e., for $n=2$, an equivalent confocal image could be produced for each OCT image.

In any optical mapping apparatus of the present invention, a feedback loop under synchronous control of the raster scanning means for providing a curvature-transversal
25 corrected image may be employed.

Moreover, in any optical mapping apparatus according to the present invention, the means to alter the length of the reference beam comprises at least one galvanometer-mirror, as noted above. Moreover, such means to alter the length of a

reference beam for the interferometer may comprise a galvanometer-mirror placed at a distance $f+\delta$ from a convergent lens, and a mirror at a distance f from the convergent lens, where f is the focal length of the convergent lens and where the incidence beam on the galvanometer-mirror is δ away from the galvanometer-mirror axis.

5 The means to alter the length of a reference beam from an interferometer may likewise comprise a galvanometer-mirror, a convergent lens, and a first mirror at distance f away from the lens, together with a second mirror to implement a double pass on the galvanometer-mirror and so as to increase the path variation. Here, the point of incidence of a beam on the galvanometer-mirror is on its axis and in the focal
10 plane of the lens; and the lens is laterally shifted in the plane of the scanned rays to ensure that, at the maximum angle of deviation, light reflected by the first mirror and reflected by the lens falls on the galvanometer-mirror.

Still further, the means to alter the length of the reference beam for the interferometer may comprise a first and second galvanometer-mirror and respective
15 first and second convergent lenses. Each converged lens is placed a distance $f+s$ from its respective galvanometer-mirror. The incidence beam on the first galvanometer-mirror is redirected to the second galvanometer-mirror, and thence to a second optical output path.

Optical mapping apparatus according to the present invention can be used to
20 generate longitudinal images by using the transversal scanning means to general a 1D sample over the object, and by replacing one of the transversal co-ordinates in the image with the longitudinal co-ordinate which corresponds to the optical path difference introduced by the longitudinal scanning means.

Still further, the apparatus may comprise a display scanning device in which a
25 vertical display performs in alternate directions which are changed at each change of a voltage ramp slope of a voltage applied to a galvanometer-mirror.

Where a galvanometer scanner is employed, the line in the raster can be such that it can be used only to create the phase modulation necessary to carry parts of the OCT image signal.

Still further, a combination of the modulation due to the galvanometer scanner giving the line in the raster, and of the modulation due to an extra phase modulator, may be employed to carry all of the OCT image signal.

Moreover, an electronic filter may be employed in a receiver such that parts of
5 the low frequency spectrum may be discarded. Frequencies up to the maximum phase modulation frequencies will, however, be passed, in keeping with the pass modulation introduced by transversal scanning of the object.

Still further, the frequency of the carrier created by the galvanometer scanner can be increased by shifting the incident optical beam away from the center of the
10 galvanometer mirror.

Optical mapping apparatus, in keeping with the present invention, can include software which will generate a transversal image O_s , with different equivalent depth resolutions. Here, transversal OCT images are combined, which have been collected at different depths. The software generated image has a depth resolution between the
15 minimum ensured by the coherence length of the optical source, and up to a maximum determined by the range of transversal images which have been collected. Each image contribution to the final image is weighted according to a predetermined profile.

Still further, a processor can be introduced into each input of a display device utilized in keeping with the present invention, so as to provide either a linear,
20 logarithmic, or squared version of an input signal thereto.

WHAT IS CLAIMED IS:

1. Optical mapping apparatus with adjustable depth resolution, comprising:

an interferometer chosen from the group consisting of fiberized interferometers and bulk interferometers, said interferometer comprising a first optical path and a second optical path leading to an object location, and to a reference reflecting assembly, respectively;

scanning means for transversely scanning an optical output from the said interferometer over a predetermined area;

interface optics for transferring an optical beam from the scanning means to an object situated at the object location and for transferring a returned optical output beam reflected and scattered from the object back to the interferometer, along said first optical path;

means for directing at least a portion of the returned optical output beams towards said reference reflecting assembly;

means to alter at least one of the first optical path and the second path, so as to introduce intensity modulation, or phase modulation, or intensity modulation and phase modulation; and

means to alter the length of at least the second optical path in steps or continuously, at a pace synchronized with said transversal scanning means;

c h a r a c t e r i z e d in that said interferometer is excited by an optical radiation source or a source with adjustable coherence length;

said apparatus further comprising comparator or analyzing means, coupled to said scanning means, for comparing a signal representative of the optical beam transferred to said object, with the output signal from said reference reflector assembly, so as to demodulate and produce an output signal from said interferometer; and

means for displaying or storing an image of at least part of said object, based on said output signal from said interferometer.

2. Optical mapping apparatus with adjustable depth resolution, comprising:
an interferometer chosen from the group consisting of fiberized interferometers and bulk interferometers, said interferometer comprising a first optical path and a second optical path leading to an object location and to a reference reflector, respectively;

a confocal optical receiver with adjustable focal depth;

an optical splitter for internally directing light returned from an object situated at said object location to said confocal optical receiver;

scanning means for transversely scanning an optical output from said interferometer over a predetermined area;

interface optics for transferring an optical beam from said scanning means to an object and for transferring an optical output beam reflected and scattered from the object back to said optical splitter through said scanning means, and from said optical splitter to both of said interferometer and said confocal optical receiver, in a ratio determined by said optical splitter;

means to alter at least one of the first optical path and the second optical path, to introduce intensity modulation, or phase modulation, or intensity modulation and phase modulation; and

means to alter the length of at least the second optical path, in steps or continuously, at a pace synchronized with transversal scanning means;

characterized in that said interferometer is excited by an optical radiation source or a source with adjustable coherence length;

said apparatus further comprising comparator or analyzing means, coupled to said scanning means, for comparing a signal representative of the optical beam transferred to said object, with the output signal from said confocal optical receiver, so as to demodulate and produce an output signal from said interferometer;

means for processing an image created by said interferometer and an image created by said confocal optical receiver; and

means for the simultaneous display of the said respective images created by said interferometer and by said confocal optical receiver.

3. Optical-mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second said source having a coherence length greater than that of the first said first source;
wherein both sources have substantially the same central wavelength.
4. Optical mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second said source having a coherence length greater than that of the first said first source;
wherein both sources have substantially the same central wavelength; and
wherein the coherence length of at least one of said optical sources is electrically adjustable to provide either a continuous range for the compound source from less than a few micrometers or a few tens of micrometers, to more than a few hundreds of micrometers, or to provide adjustability on some subintervals.
5. Optical mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second said source having a coherence length greater than that of the first said first source;
wherein both sources have substantially the same central wavelength;
wherein said optical source comprises an electronic unit, for changing the ratio of the powers of said two radiation sources; and
wherein, when changing the ratio of the powers of said two superposed radiation sources, said electronic unit ensures that the overall intensity is kept constant, or that the bias intensity in the final image is kept constant.
6. Optical mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very

short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second said source having a coherence length greater than that of the first said first source;

wherein both sources have substantially the same central wavelength; and

wherein said optical source comprises an electro-optic element for balancing the contribution of the two component sources in the final output beam.

7. Optical mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second said source having a coherence length greater than that of the first said first source;

wherein both sources have substantially the same central wavelength;

wherein said optical source comprises an electro-optic element for balancing the contribution of the two component sources in the final output beam; and

wherein said electro-optic element is an electrically controllable directional coupler.

8. Optical mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second said source having a coherence length greater than that of the first said first source;

wherein both sources have substantially the same central wavelength; and

wherein said optical source comprises two first fibers, each said first fiber being arranged for transmitting light from a respective optical source, and a second fiber for collecting light from said source fibers, said second fiber being translatable between said first fibers.

9. Optical mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second source having a coherence length greater than that of the first said first source;

wherein both sources have substantially the same central wavelength;
said optical mapping apparatus further comprising a translatable collecting fiber for collecting light from said optical sources.

10. Optical mapping apparatus according to claim 1 or 2, wherein said optical source with adjustable coherence length is a multi-electrode laser diode, a DFB laser, or a superluminescent diode.

11. Optical mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second said source having a coherence length greater than that of the first said first source;

wherein both sources have substantially the same central wavelength; and

wherein said optical source with adjustable coherence length is a subnanosecond tunable optical source which is adapted to be tuned under subnanosecond electrical pulse control in a bandwidth for which the associated correlation profile width secures a predetermined depth resolution.

12. Optical mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second said source having a coherence length greater than that of the first said first source;

wherein both sources have substantially the same central wavelength;

wherein said first optical source of largest bandwidth is modulated in intensity at a first frequency, and the second source of narrowest bandwidth is modulated in intensity at a second frequency, said first and second frequencies being different, and their ratio being an irrational numeral, and wherein said representative of the optical beam transferred to said object signal is sent to a first receiver tuned on said first frequency and to a second receiver tuned on a second frequency, so as to select the corresponding images, where the first corresponding image has a very narrow

sectioning interval given by said first receiver tuned on said the first frequency, and where the second corresponding image has a wider sectioning interval given by said second receiver tuned on said second frequency; and

wherein said first and second corresponding images are displayed simultaneously by way of a two input display device.

13. Optical mapping apparatus according to claim 2, wherein said optical source is broadband.

14. Optical mapping apparatus according to claim 2, wherein said optical splitter is a bulk beamsplitter.

15. Optical mapping apparatus according to claim 2, wherein said optical splitter is a fiberized directional coupler terminated on a pigtailed photodetector provided on said optical confocal receiver, and wherein the fiber input of the directional coupler acts as the aperture of said confocal optical receiver, and said optical splitter is part of said first optical path of said interferometer.

16. Optical mapping apparatus according to claim 2, wherein the image given by said confocal optical receiver is used in the storage process of the image given by an OCT channel, to compensate during its acquisition, for the transversal object movement.

17. Optical mapping apparatus according to claim 2, wherein the means for processing an image can perform mathematical operations in a pixel-by-pixel format using the interferometer image and the confocal optical receiver image.

18. Optical mapping apparatus according to claim 16, wherein the means for processing images can perform mathematical operations in a pixel-by-pixel format using the image obtained by said storage process.

19. Optical mapping apparatus according to claim 14, wherein said confocal receiver comprises an adjustable pinhole behind a lens or between lenses and a photodetector, and the focal depth interval is adjustable independently of the said interferometer.
20. Optical mapping apparatus according to claim 14, wherein said confocal receiver comprises a fiber pigtail terminated on a photodetector.
21. Optical mapping apparatus according to claim 1 or 2, wherein there is a reference beam for said interferometer, and wherein said apparatus is further provided with a blocking means to block said reference beam, and wherein, when said blocking means is activated, it synchronously switches the input of the displaying device to the output of a high gain amplifier for the signal representative of the optical beam transferred to said object.
22. Optical mapping apparatus according to claim 1 or 2, wherein there is a reference beam for said interferometer, and wherein said apparatus is further provided with a blocking means to block said reference beam, and wherein, when said blocking means is activated, it synchronously switches the input of the displaying device to the output of a high gain amplifier for the signal representative of the optical beam transferred to said object; and
wherein, when said photodetectors are avalanche, their gain is switched automatically by a reference power via the voltage drop on series resistors connected therewith, said optical mapping apparatus is switched between a confocal regime of operation and an OCT regime of operation.
23. Optical mapping apparatus according to claim 1 or 2, wherein there is a reference beam for said interferometer, and wherein said apparatus is further provided with a blocking means to block said reference beam, and wherein, when said blocking means is activated, it synchronously switches the input of the displaying device to the

output of a high gain amplifier for the signal representative of the optical beam transferred to said object; and

wherein, when said interferometer is a bulk interferometer, the depth resolution of the image obtained with the reference arm blocked can be adjusted by varying the numerical aperture of optics preceding a photodetector, when the photodetector is used, or by simultaneously varying the numerical apertures of optics preceding two photodetectors when balance detection is employed, said numerical apertures being varied by adjusting either the focal length of the lenses or by adjusting the diameter of the pinhole in the optics preceding the photodetector, or photodetectors when balance detection is used.

24. Optical mapping apparatus according to claim 19, wherein said optical source is broadband, and wherein the depth resolution in a final image produced by said optical mapping apparatus is adjustable by choosing a step chosen from the group of steps consisting of:

- (i) adjusting the depth sectioning interval of the image produced by the confocal optical receiver; and
- (ii) balancing the amplitudes of an interferometer image signal and of an optical confocal receiver signal sent to display means, so as to provide an adjustable resolution depth from a minimum given by the coherence length of the broadband source to a maximum given by the confocal optical receiver.

25. Optical mapping apparatus according to claim 15, wherein said optical source is broadband;

wherein the depth resolution in a final image produced by said optical mapping apparatus is adjustable by balancing the amplitudes of an interferometer image signal and of an optical confocal receiver signal sent to a display means, so as to provide an adjustable resolution depth from a minimum given by the coherence length of the broadband source to a maximum given by the confocal optical receiver.

26. Optical mapping apparatus according to claim 19, wherein the depth resolution in the final image or in the two or three images produced by the apparatus is adjustable by choosing a step chosen from the group of steps consisting of:

(i) adjusting the depth sectioning interval of a confocal optical receiver image;

(ii) varying the sectioning interval of one of the interferometer images by changing the coherence length of the source; and

(iii) weighting the contributions of the interferometer and confocal optical receiver in a compound image, so as to provide an adjustable resolution depth from a minimum given by the minimum coherence length of the said first source to a maximum given by either the confocal optical receiver or the maximum coherence length of the said second source.

27. Optical mapping apparatus according to claim 1 or 2, wherein said optical source comprises two superposed radiation sources, one first said source having a very short coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$, and the other second said source having a coherence length greater than that of the first said first source;

wherein both sources have substantially the same central wavelength;

wherein said first optical source of largest bandwidth is modulated in intensity at a first frequency, and the second source of narrowest bandwidth is modulated in intensity at a second frequency, said first and second frequencies being different, and their ratio being an irrational numeral, and wherein said signal representative of the optical beam transferred to said object is sent to a first receiver tuned on said first frequency and to a second receiver tuned on a second frequency, so as to select the corresponding images, where the first corresponding image has a very narrow sectioning interval given by said first receiver tuned on said the first frequency, and where the second corresponding image has a wider sectioning interval given by said second receiver tuned on said second frequency;

wherein said first and second corresponding images are displayed simultaneously by way of a two input display device; and

wherein the depth resolution in the final image or in the two or three images produced by the apparatus is adjustable by choosing a step chosen from the group of steps consisting of:

(i) adjusting the depth sectioning interval of a confocal optical receiver image;

(ii) varying the sectioning interval of one of the interferometer images by changing the coherence length of the source or of one of the sources; and

(iii) weighting the contributions of the interferometer and confocal optical receiver in a compound image, so as to provide an adjustable resolution depth from a minimum given by the minimum coherence length of the said first source to a maximum given by either the confocal optical receiver or the maximum coherence length of the said second source.

28. Optical mapping apparatus according to claim 15, wherein the depth resolution in a final image produced by the apparatus is adjustable by choosing a step from the group of steps consisting of:

(i) varying the sectioning interval of an image produced by the interferometer by changing the coherence length of the source; and

(ii) weighting the contributions of the interferometer and confocal optical receiver, so as to provide an adjustable resolution depth from a minimum given by the minimum coherence length of the source to a maximum given by the confocal optical receiver.

29. Optical mapping apparatus according to claim 2, wherein said optical splitter has an optimized splitting ratio, so as to ensure optimal signal-to-noise ratios in images generated by both the interferometer and the optical confocal receiver.

30. Optical mapping apparatus with adjustable depth resolution, comprising:
an interferometer chosen from the group consisting of fiberized interferometers and bulk interferometers, wherein said interferometer is excited by an

optical source chosen from the group consisting of broadband optical sources and sources having adjustable coherence length;

wherein said interferometer comprises a first optical path and a second optical path leading to an object location, and to a reference reflector assembly, respectively;

an optical element for producing an enlargement of the correlation function of the optical source when placed in either of said first path or said second path;

scanning means for transversely scanning an optical output from said interferometer over a predetermined area;

interface optics, for transferring an optical beam from said scanning means to an object situated at said object location, and for transferring a returned optical output beam reflected and scattered from said object back to said interferometer, along said first optical path;

means for directing at least a portion of the returned optical output beams towards said reference reflector assembly; and

means to alter at least one of said first optical path and said second optical path, to introduce intensity modulation, or phase modulation, or intensity modulation and phase modulation;

c h a r a c t e r i z e d in that said interferometer is excited by an optical source chosen from the group consisting of broadband optical sources and sources having adjustable coherence length;

said apparatus further comprising comparator or analyzing means, coupled to said scanning means, for comparing a signal representative of the optical beam transferred to said object, with the output signal from said reference reflector assembly, so as to demodulate and produce an output signal from said interferometer;

means for longitudinal scanning, to alter the length of the first optical path or the second optical path in steps or continuously, at a pace synchronized with transversal scanning means; and

means for displaying or storing an image of at least part of said object based on said output signal from said interferometer.

31. Optical mapping apparatus according to claim 30, wherein said optical element for enlarging the correlation profile of the optical source is a dispersive element which causes an increase in the associated coherence length.

32. Optical mapping apparatus according to claim 30, wherein said optical element for enlarging the correlation profile of the optical source is a multi-step echelon.

33. Optical mapping apparatus according to claim 31, wherein said dispersive element can be gradually introduced into the first or second path for a continuous adjustment of the coherence length and consequently of the depth resolution in an image generated by said optical mapping apparatus.

34. Optical mapping apparatus with adjustable depth resolution, comprising:
at least two interferometers excited by an optical source consisting of broadband optical source on a source having adjustable coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$;

wherein each of said interferometers comprises an at least partly common first optical path leading to an object location, and a respective second optical path for each interferometer, wherein each of said second optical paths leads to a respective reference reflector assembly;

at least one device for producing an enlargement of the correlation function of the source when placed in at least one of said second optical paths;

scanning means for transversely scanning an optical output from said interferometers over a predetermined area;

interface optics for transferring an optical beam from said scanning means to an object situated at the object location, and for transferring an optical output beam reflected and scattered from the object back to said interferometers, along said first optical path;

means for directing at least a portion of the returned optical output beam towards said reference reflector assembly; and

means to alter at least one of said first optical path, and said second optical path, to introduce intensity modulation, phase modulation, or intensity modulation and phase modulation;

c h a r a c t e r i z e d in that each of said at least two interferometers is excited by an optical source consisting of broadband optical sources or a source having adjustable coherence length in the range of $10\mu\text{m}$ to $300\mu\text{m}$;

said apparatus further comprising comparator or analyzing means, coupled to said scanning means, for comparing a signal representative of the optical beam transferred to said object, with the output signal from said respective reference reflector assembly, so as to demodulate and produce an output signal from each said interferometers;

longitudinal scanning means to alter the length of said first optical path or said second optical path in each interferometer simultaneously in steps or continuously, at a pace synchronized with transversal scanning means; and

means for displaying or storing two images of at least part of said object based on said output signal from each said interferometer.

35. Optical mapping apparatus according to claim 34, wherein said first optical path is completely shared by said interferometers, and wherein said analyzing means uses a single photo receiver for all of said interferometers, and for each said second optical path; and

wherein said optical mapping apparatus comprises a phase modulator in each interferometer, where each respective phase modulation is driven at a different frequency sufficiently distant apart from the other respective phase modulation frequencies for said analyzing means to be able to separate the respective signals in said interferometers, by means of subsequent frequency band pass filtering.

36. Optical mapping apparatus according to claim 34 or 35, further comprising means for processing signals in said interferometers using mathematical operations in a pixel-by-pixel format in a controllable ratio using respective images created by each said interferometer.

37. Optical mapping apparatus according to claim 34 or 35, wherein said optical element for enlarging the correlation profile of said optical source can be gradually introduced into the second path of one of the interferometers, for continuous adjustment of the depth resolution of an image provided by that interferometer.

38. Optical mapping apparatus according to claim 34 or 35, wherein said optical element for enlarging the correlation profile of the optical source is a dispersive element which causes an increase in the associated coherence length.

39. Optical mapping apparatus according to claim 34 or 35, wherein said optical element for enlarging the correlation profile of the optical source is a multi-step echelon.

40. Optical mapping apparatus according to claim 34 or 35, wherein an image in the one of the said interferometers which has the poorest depth resolution, obtained by using said optical element for enlarging the correlation profile, is used in a process for storing an image with the best depth resolution, obtained using another interferometer with no such optical element, in order to compensate for transversal object movement during image acquisition.

41. Optical mapping apparatus according to claim 1, 2, 30, or 34, comprising a feedback loop under synchronous control of said scanning means for providing a curvature-corrected transversal image.

42. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein the means to alter the length of the reference beam comprises at least one galvanometer-mirror.

43. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein the means to alter the length of the reference beam comprises at least one galvanometer-mirror; and

wherein said means to alter the length of a reference beam for said interferometer comprises a galvanometer-mirror placed at a distance $f+\delta$ from a convergent lens, and a mirror at a distance f from said convergent lens, where f is the focal length of the convergent lens and where the incidence beam on the galvanometer-mirror is δ away from the galvanometer-mirror axis.

44. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein the means to alter the length of the reference beam comprises at least one galvanometer-mirror;

wherein the means to alter the length of a reference beam for said interferometer comprises a galvanometer-mirror, a convergent lens, and a first mirror at a distance f away from the lens, and a second mirror to implement a double pass on the galvanometer-mirror and so as to increase the path variation;

wherein the point of incidence of a beam on the galvanometer-mirror is on its axis and in the focal plane of the lens; and

wherein the lens is laterally shifted in the plane of the scanned rays to ensure that, at the maximum angle of deviation, light reflected by said first mirror and refracted by the lens falls on said galvanometer-mirror.

45. Optical mapping apparatus according to claim 34, where said optical mapping apparatus can be used to generate longitudinal images by using said transversal scanning means to generate a 1D sample over the object, and by replacing one of the

transversal coordinates in the image with the longitudinal coordinate corresponding to the optical path difference introduced by said longitudinal scanning means.

46. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein the means to alter the length of the reference beam comprises at least one galvanometer-mirror;

said optical mapping apparatus further comprising a display scanning device in which a vertical display thereof performs in alternate directions which are changed at each change of a voltage ramp slope of a voltage applied to said galvanometer.

47. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein the means to alter the length of the reference beam comprises at least one galvanometer-mirror;

said optical mapping apparatus further comprising a display scanning device in which a vertical display thereof performs in alternate directions which are changed at each change of a voltage ramp slope of a voltage applied to said galvanometer; and

wherein the galvanometer scanner gives a line in a raster which can be used only to create the phase modulation to carry parts of the OCT image signal.

48. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein the means to alter the length of the reference beam comprises at least one galvanometer-mirror;

said optical mapping apparatus further comprising a display scanning device in which a vertical display thereof performs in alternate directions which are changed at each change of a voltage ramp slope of a voltage applied to said galvanometer;

wherein the galvanometer scanner gives a line in a raster which can be used only to create the phase modulation to carry parts of the OCT image signal; and

wherein a combination of the modulation due to the galvanometer scanner, and of the modulation due to an extra phase modulator, is employed to carry all of the OCT image signal.

49. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein the means to alter the length of the reference beam comprises at least one galvanometer-mirror;

said optical mapping apparatus further comprising a display scanning device in which a vertical display thereof performs in alternate directions which are changed at each change of a voltage ramp slope of a voltage applied to said galvanometer;

wherein the galvanometer scanner gives a line in a raster which can be used only to create the phase modulation to carry parts of the OCT image signal; and

wherein an electronic filter in a receiver may discard parts of the low frequency spectrum, and pass frequencies up to the maximum phase modulation frequencies resulting by the pass modulation introduced by transversal scanning of the object.

50. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein the means to alter the length of the reference beam comprises at least one galvanometer-mirror;

said optical mapping apparatus further comprising a display scanning device in which a vertical display thereof performs in alternate directions which are changed at each change of a voltage ramp slope of a voltage applied to said galvanometer;

wherein the galvanometer scanner gives a line in a raster which can be used only to create the phase modulation to carry parts of the OCT image signal; and

wherein the frequency of the carrier created by the said galvanometer scanner can be increased by shifting the incident optical beam away from the center of the galvanometer mirror.

51. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein said apparatus includes software which can generate a transversal image O_s with different equivalent depth resolutions, by combining transversal OCT images collected at different depths, wherein said software generated image has a depth resolution between

the minimum ensured by the coherence length of the optical source up to a maximum determined by the range of transversal images which have been collected; and

wherein each image contribution to the final image is weighted according to a predetermined profile.

52. Optical mapping apparatus according to claim 1, 2, 30, or 34, where a processor can be introduced in each input of a display device to provide either a linear, logarithmic, or squared version of an input signal thereto.

53. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein the means to alter the length of the reference beam comprises at least one galvanometer-mirror; and

wherein said means to alter the length of a reference beam for said interferometer comprises a first galvanometer-mirror, a first convergent lens, a second galvanometer-mirror, and a second convergent lens, where each respective lens is placed at a distance $f+s$ from the respective galvanometer-mirror, wherein f is the focal length of each respective convergent lens;

wherein the incidence beam on the first galvanometer-mirror is redirected to said second galvanometer-mirror and thence to a second optical output path.

54. Optical mapping apparatus according to claim 29, wherein said optical source is broadband; and

wherein the depth resolution in a final image produced by said optical mapping apparatus is adjustable by balancing the amplitudes of an interferometer image signal and of an optical confocal receiver signal sent to a display means, so as to provide an adjustable resolution depth from a minimum given by the coherence length of the broadband source to a maximum given by the confocal optical receiver.

55. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein said comparator or analyzing means includes two inputs for analog signals applied thereto

and one analog output signal, an input for receiving control signals from a computer, at least one analog to digital convertor for converting at least one of the two analog signals input thereto for digital manipulation under the control of said computer and so as to produce a weighted output signal, and a comparator for comparing a weighted output signal from said at least one analog to digital convertor to a signal representative of the other of the two analog input signals so as to produce an output analog signal from said comparator or analyzing means which is a function of said at least one weighted output signal and said signal representative of the other of said two analog input signals.

56. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein said comparator or analyzing means includes two inputs for analog signals applied thereto and one analog output signal, an input for receiving control signals from a computer, a multiplying digital to analog convertor capable of receiving said two analog input signals and outputting said one analog output signal under the control of said computer, wherein each analog input signal is converted to a digital signal, at least one of the resultant digital signals is multiplied by a weighting factor under the control of said computer, and the product signals are added and converted to analog signal so as to produce said analog output signal.

57. Optical mapping apparatus according to claim 1, 2, 30, or 34, wherein said comparator or analyzing means includes two inputs for analog signals applied thereto and one analog output signal, an input for receiving control signals from a computer, at least one analog multiplier under the control of the computer acting on at least one of the two input analog signals to produce a multiplier product signal having a value in the range of $1/n$ to $n-1/n$ times the original input analog signal being acted upon, where n is a whole integer from 2 to 256, and comparator means for comparing the multiplier product signal to a signal representative of the other of the two analog input signals so as to produce an output analog signal from said comparator or analyzing

means which is a function of said at least one weighted output signal and said signal representative of the other of said two analog input signals.

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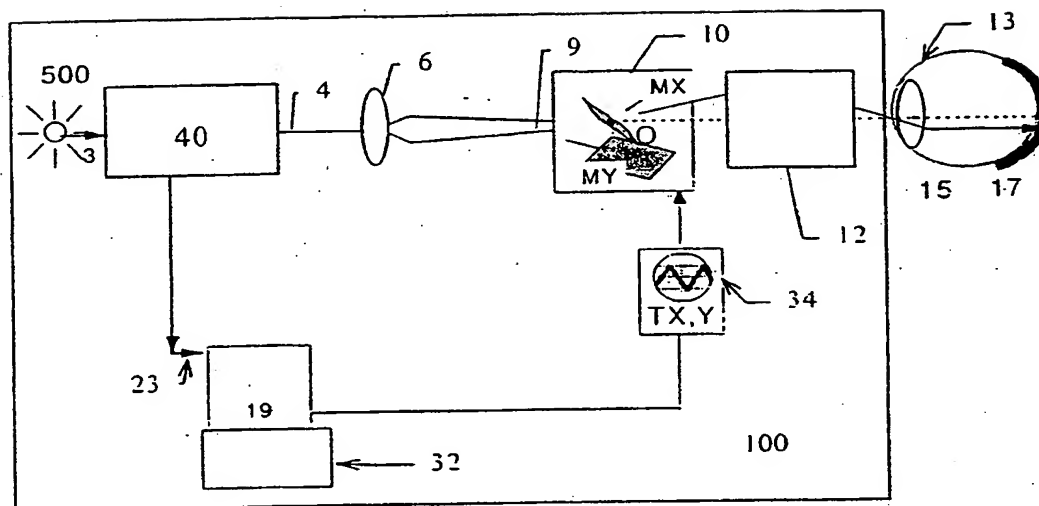


Figure 2

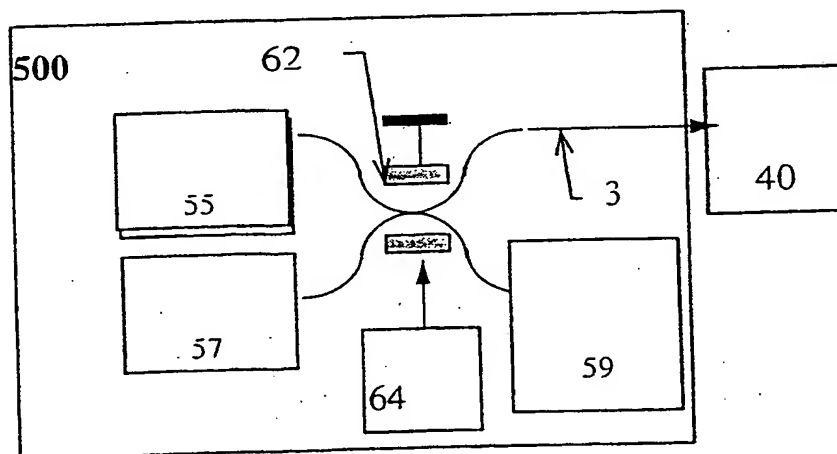


Figure 3

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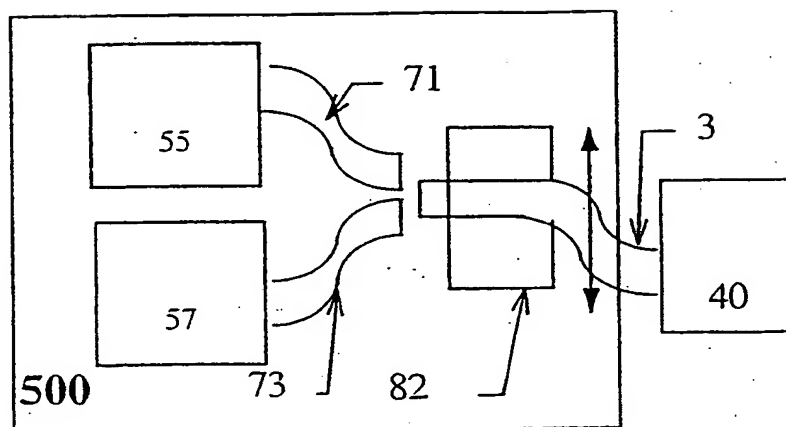


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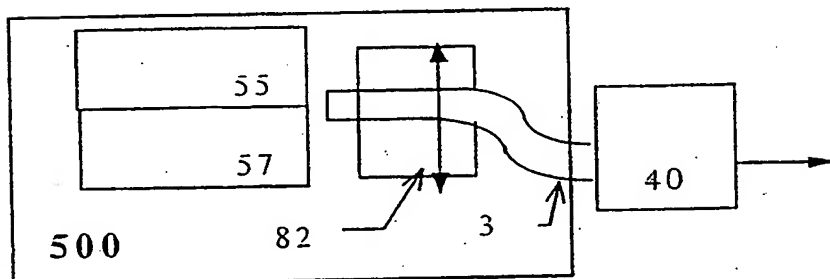


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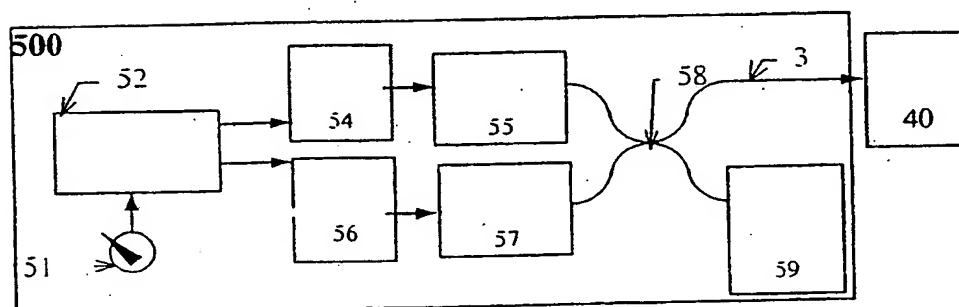


Figure 8

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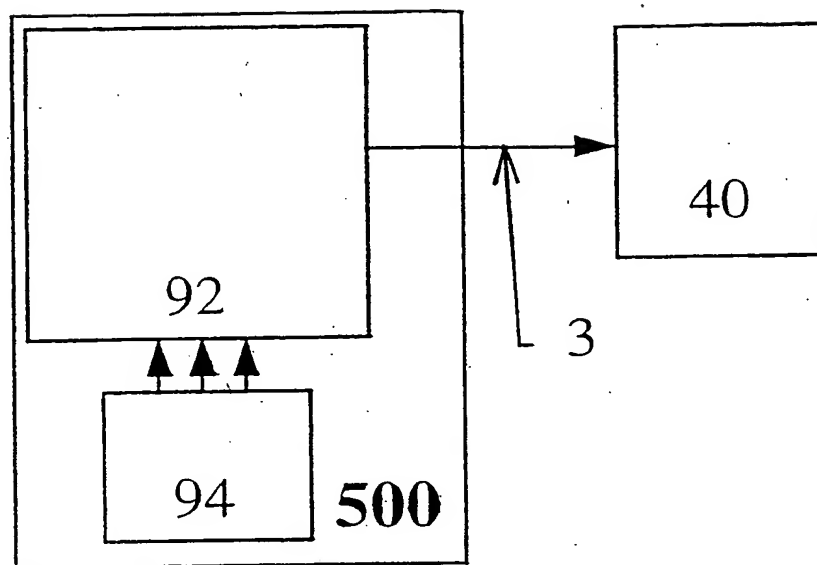


Figure 6

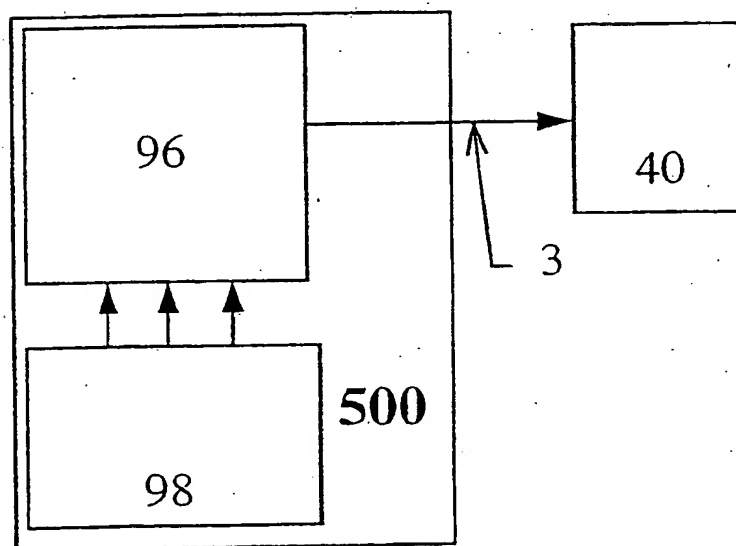


Figure 7

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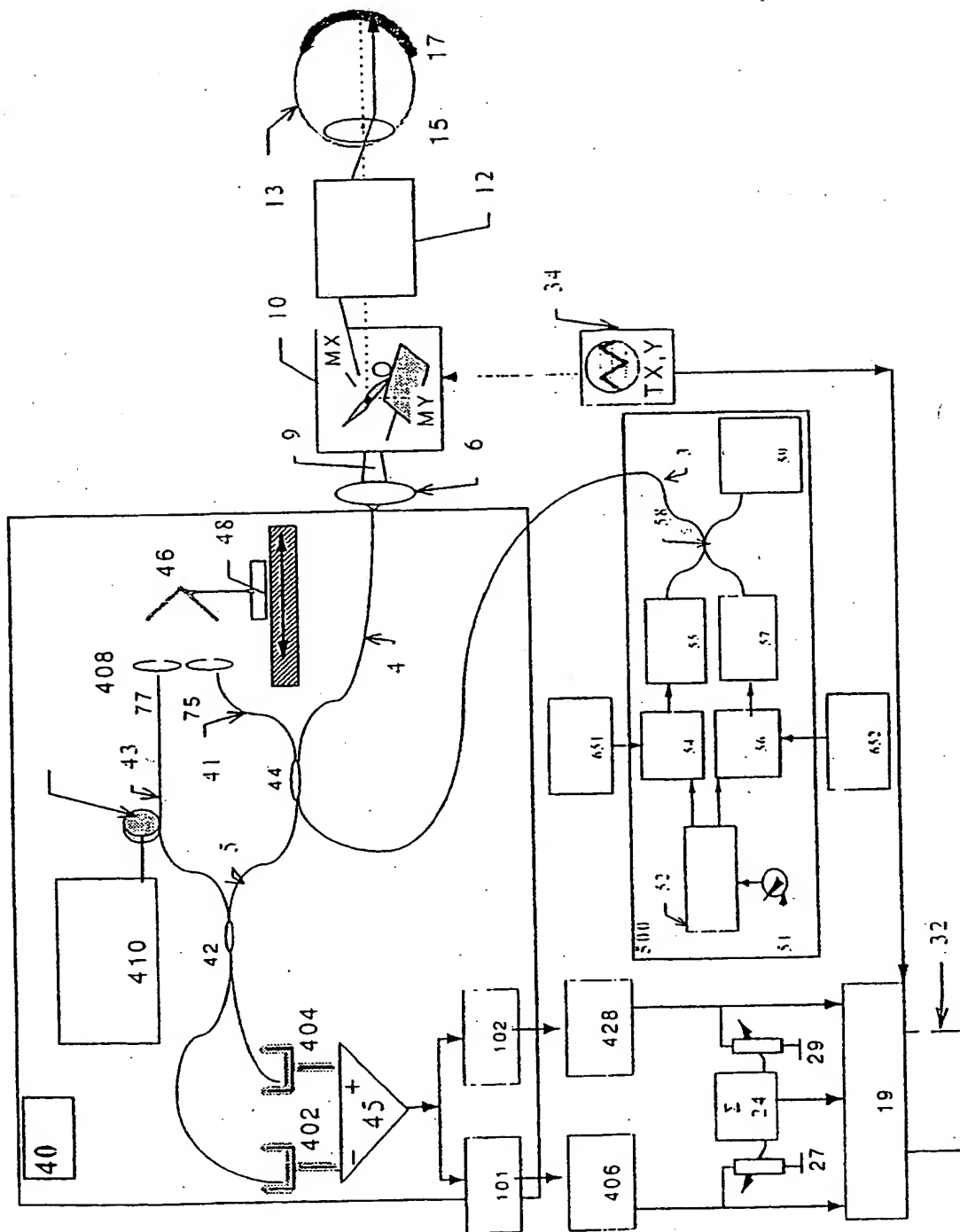


Figure 9

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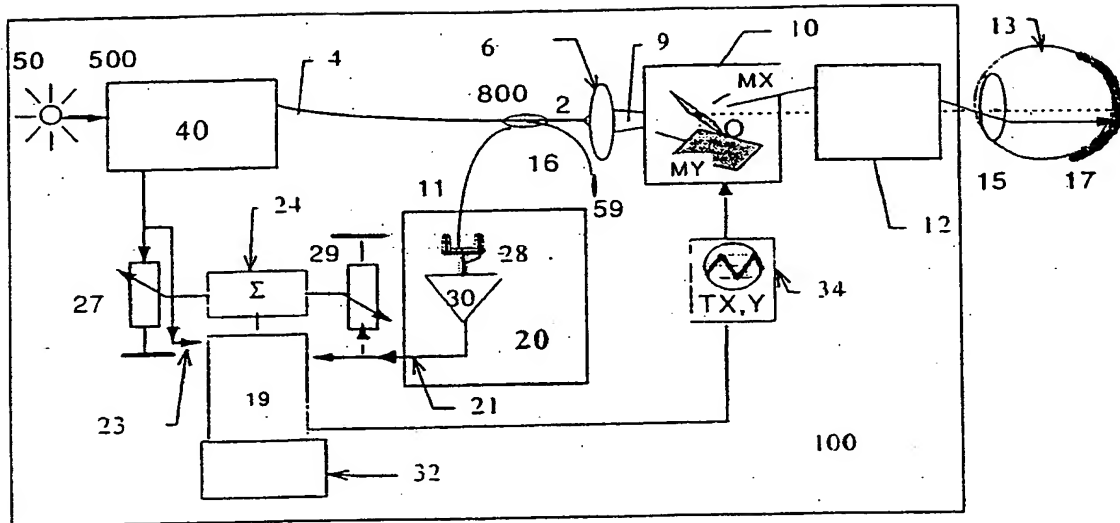


Figure 13

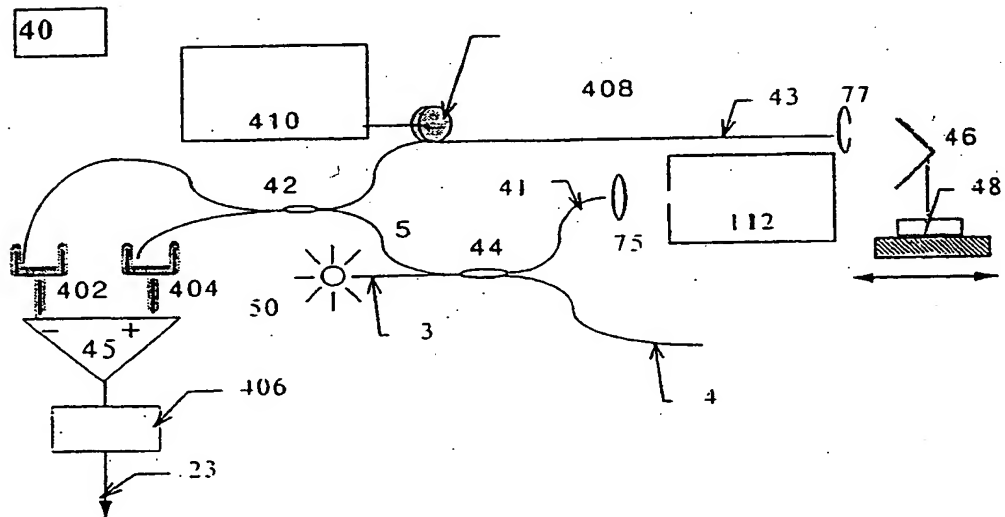
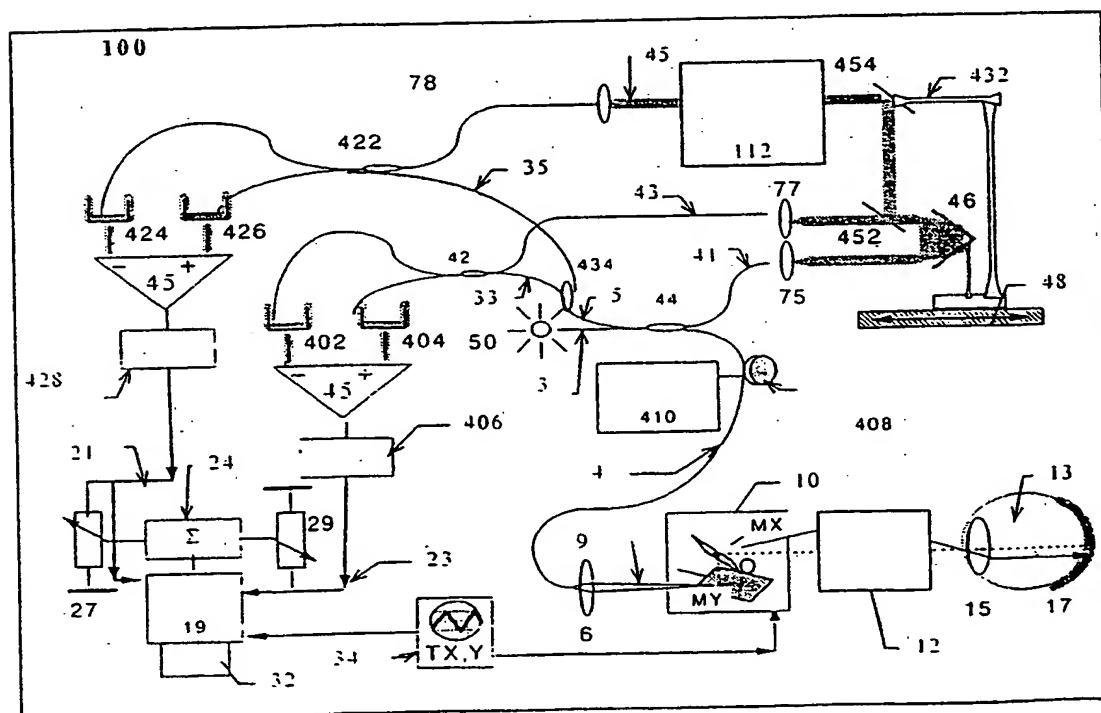
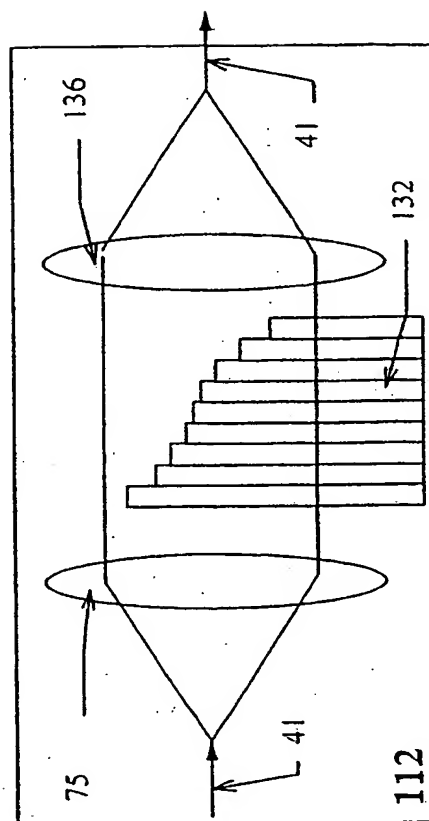
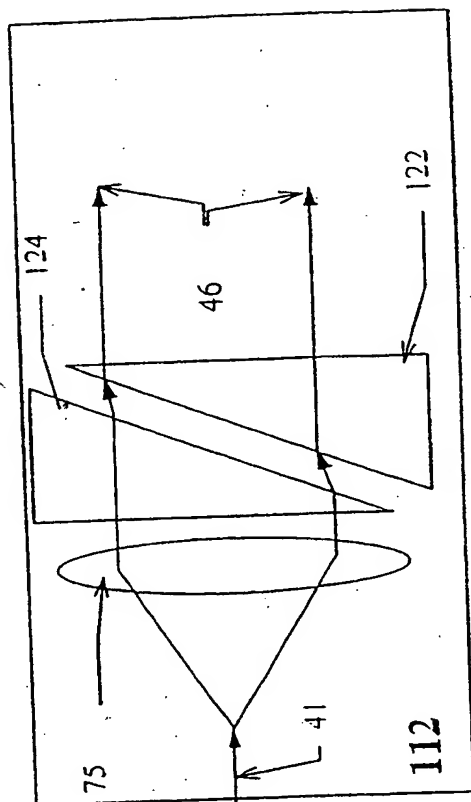


Figure 15

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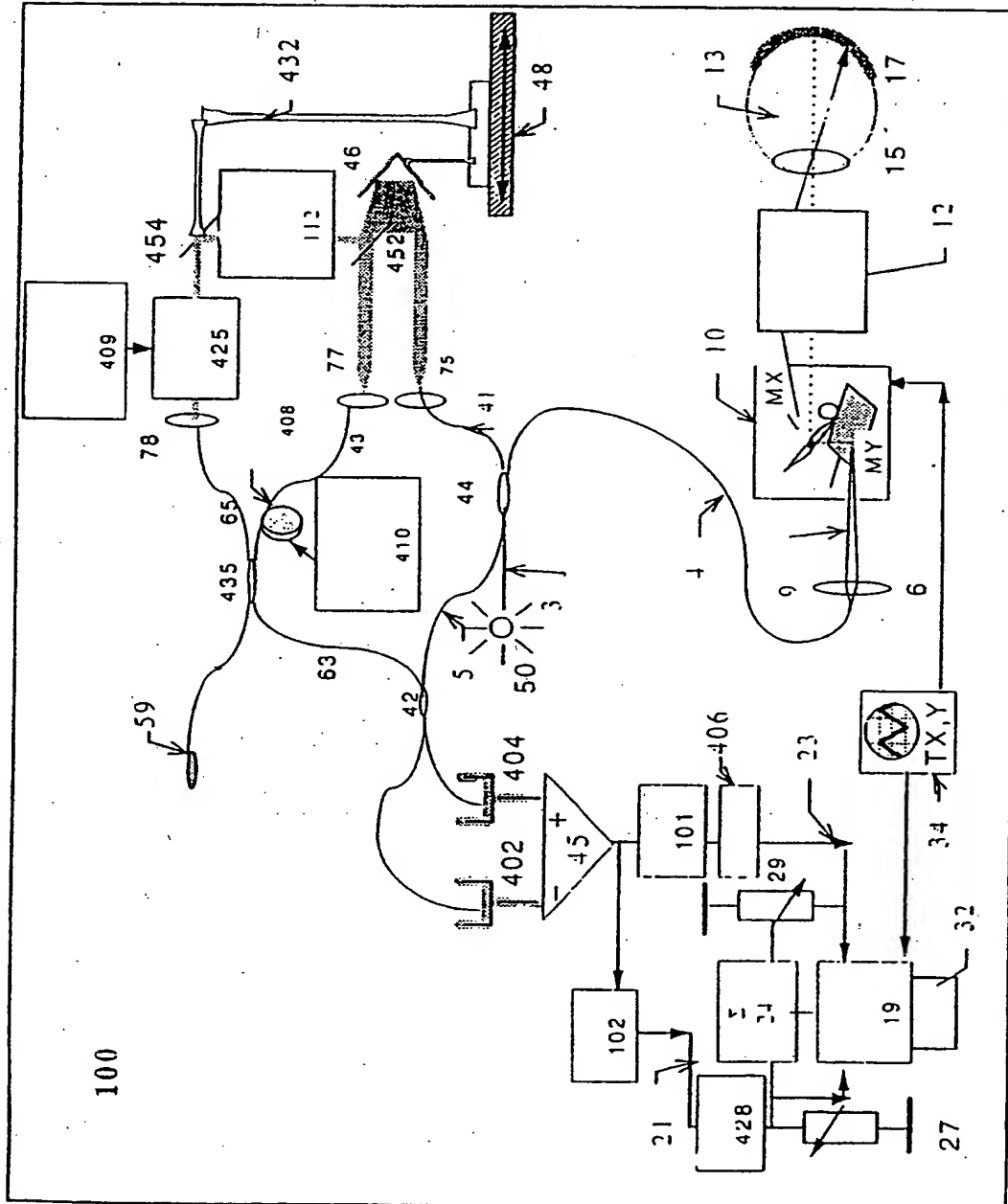


Figure 19

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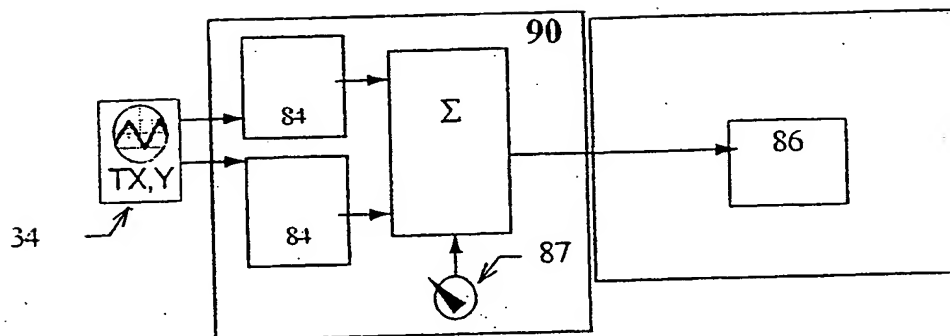


Figure 20

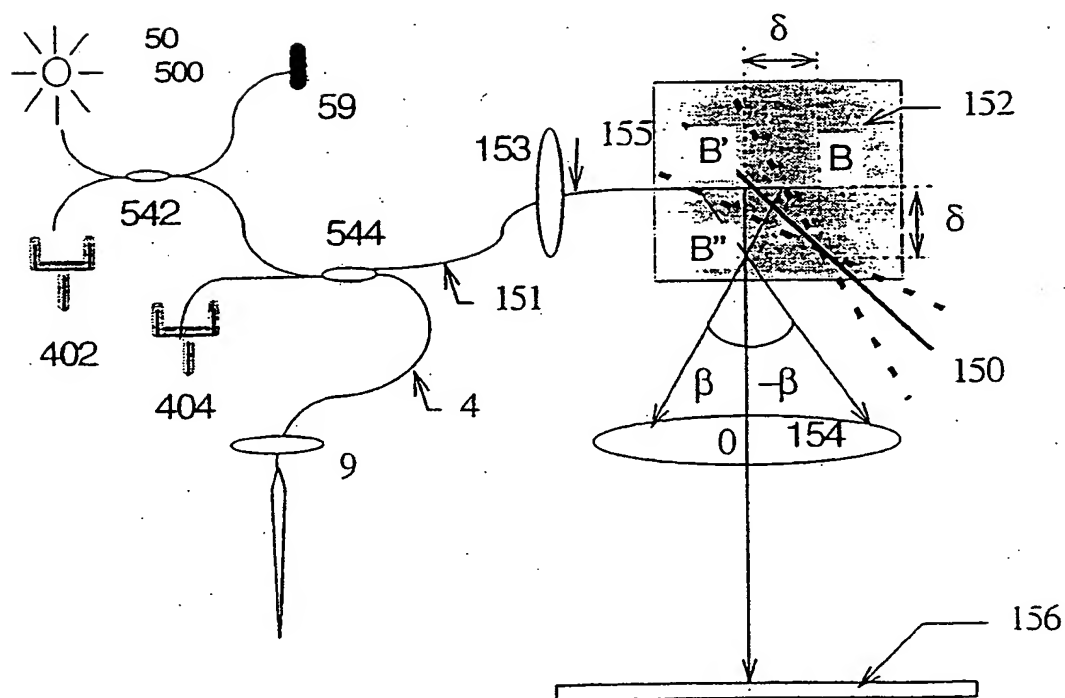


Figure 21

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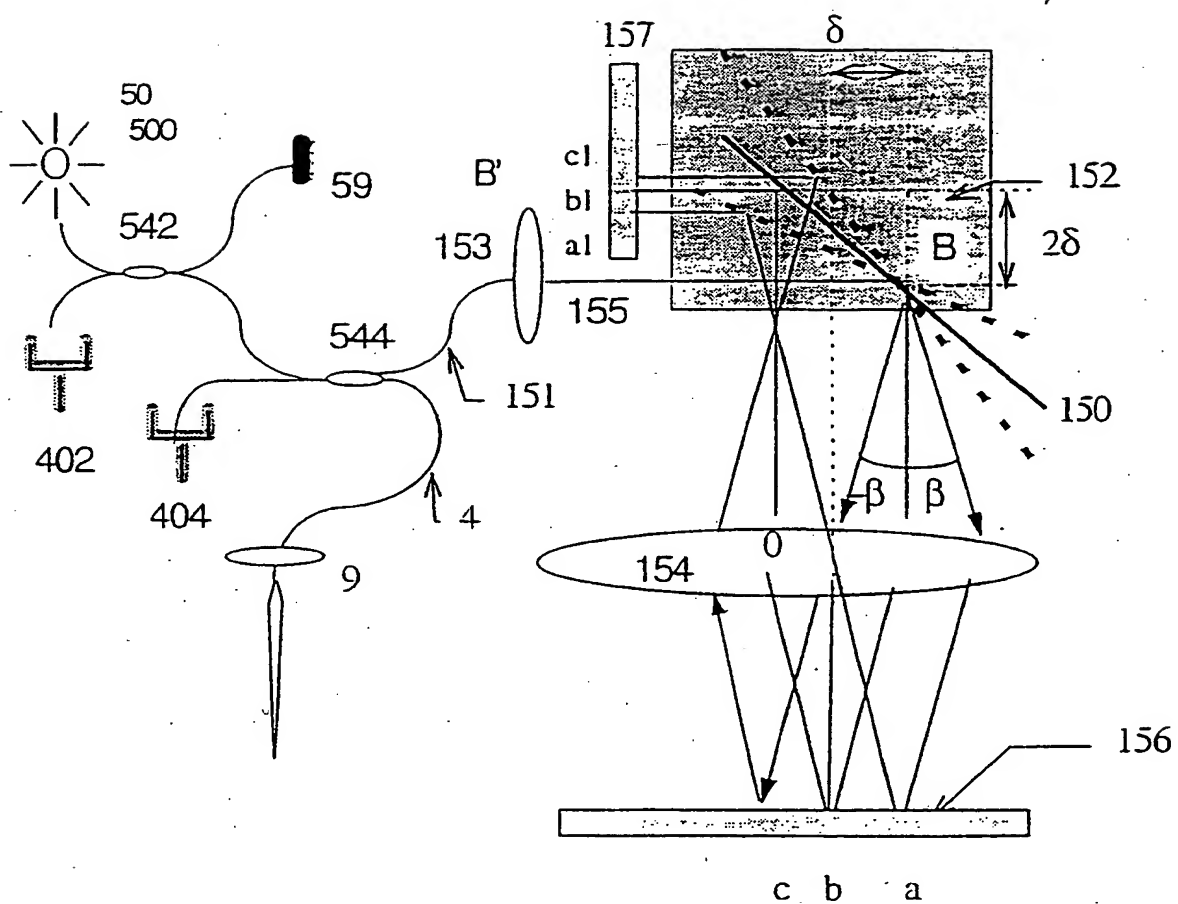


Figure 22

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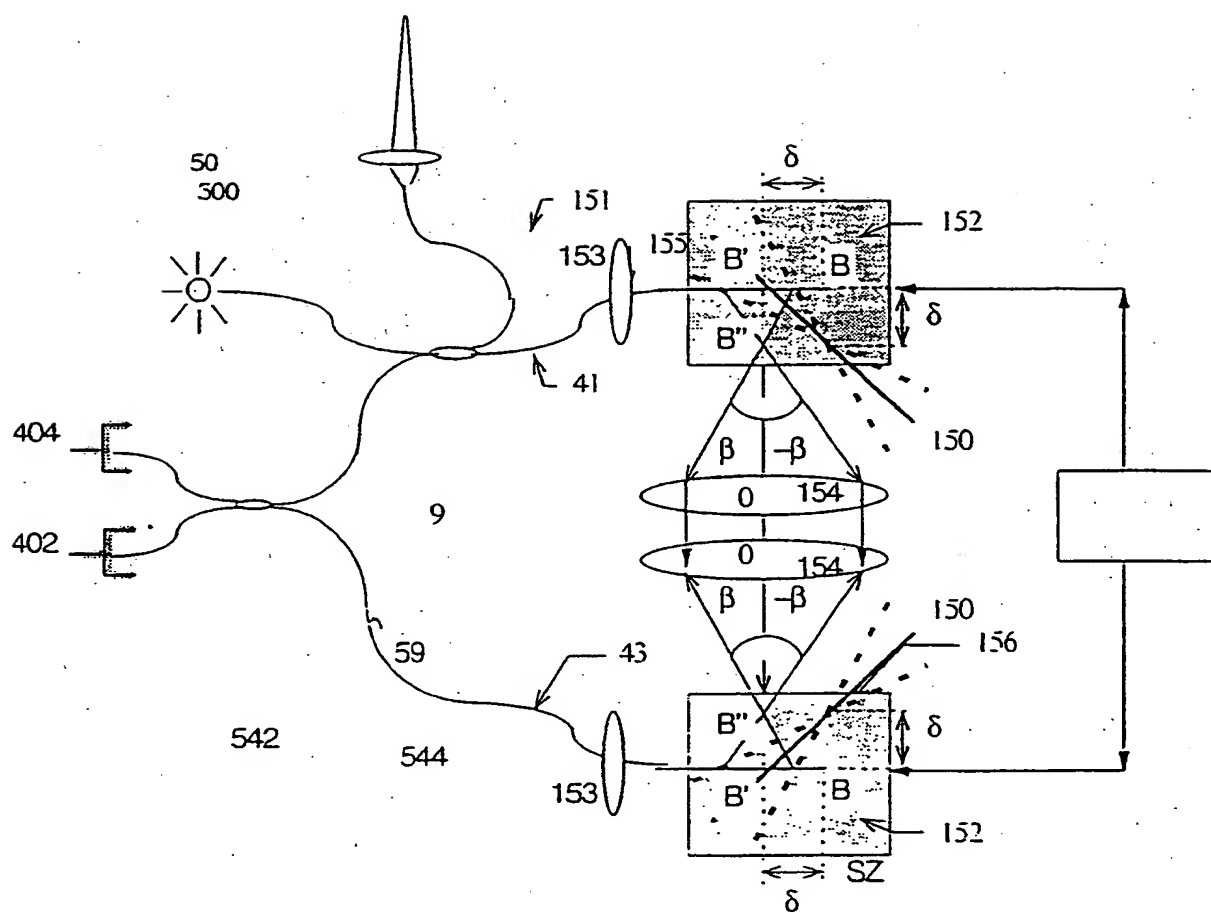
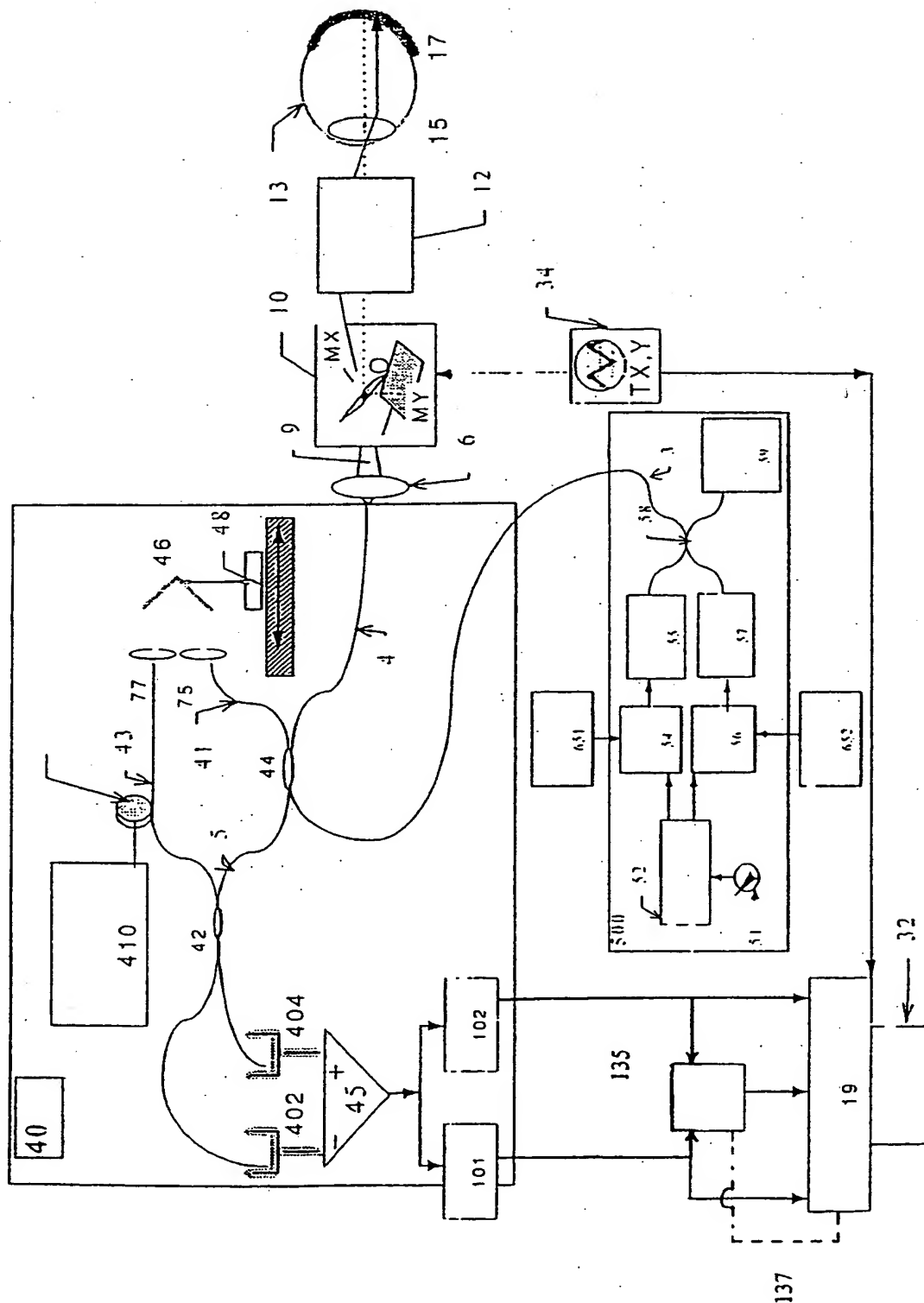


Figure 23

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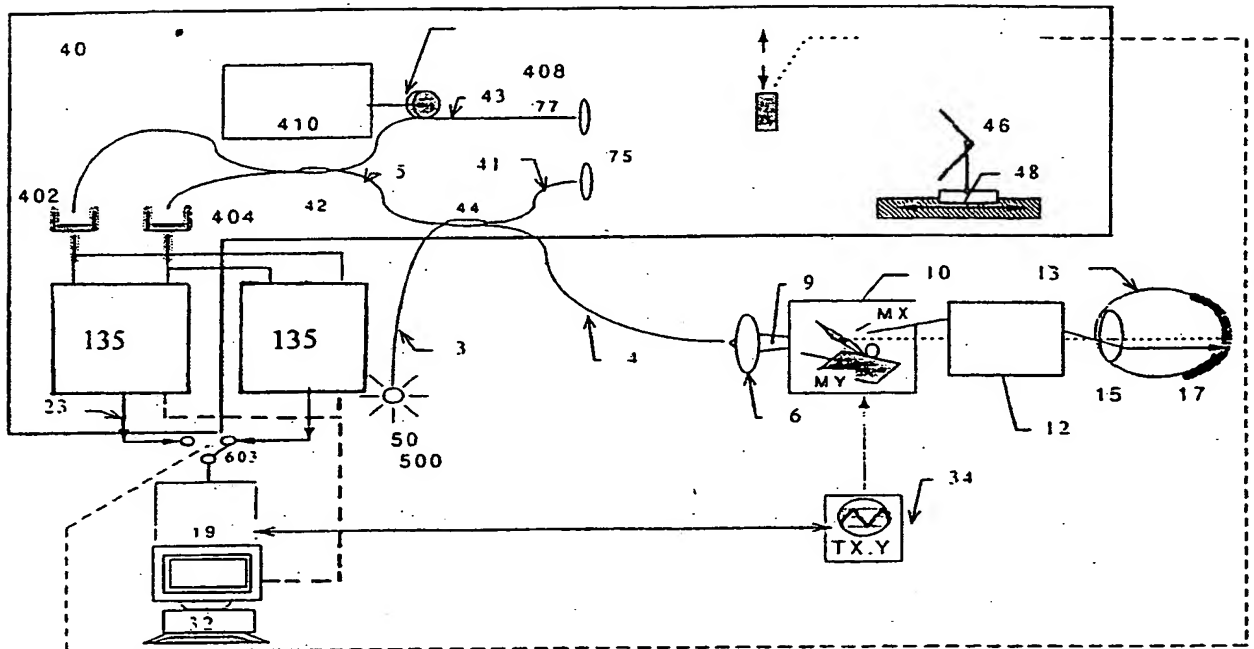
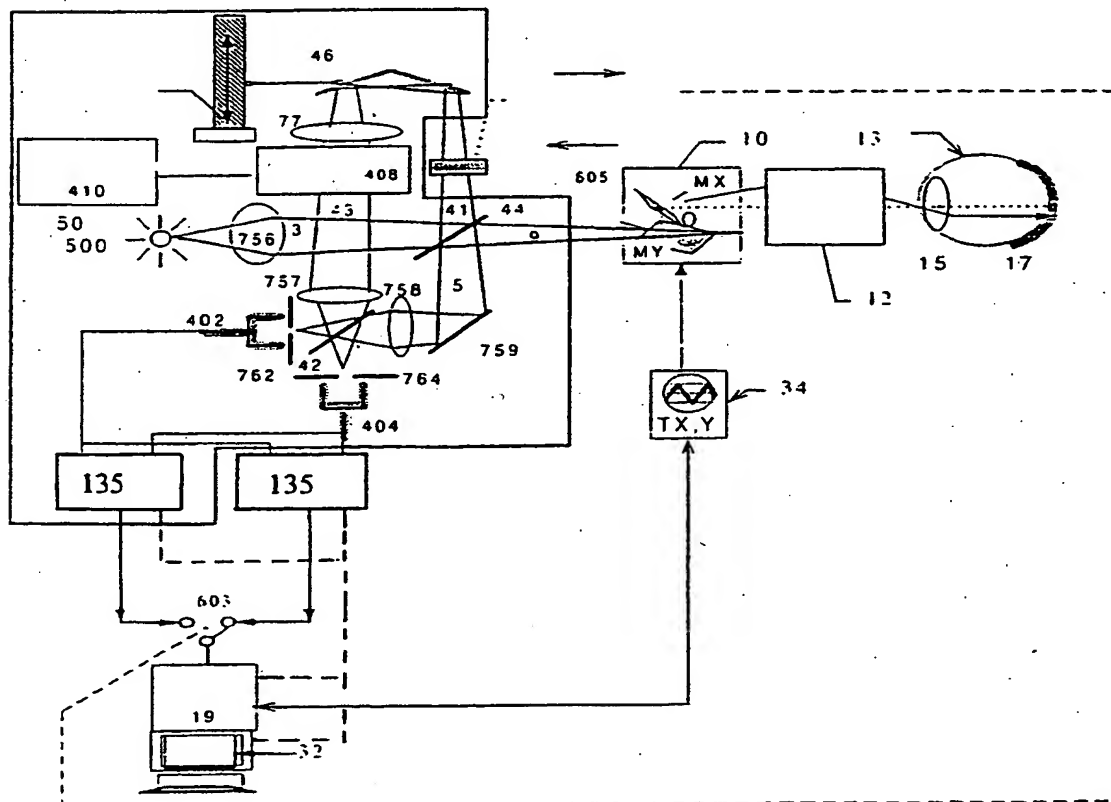


Figure 14 C



INTERNATIONAL SEARCH REPORT

International Application No
PCT/CA 99/01174

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 G01B11/24 G01B9/02

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 G01B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

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C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 97 32182 A (MASSACHUSETTS INSTITUTE OF TECHNOLOGY) 4 September 1997 (1997-09-04) page 6, line 2 -page 25, line 29; figures 3-8,16-19	1,2,30, 34
A	WO 99 22198 A (ÉCOLE POLYTECHNIQUE FÉDÉRALE DE LAUSANNE) 6 May 1999 (1999-05-06) page 5, line 2 -page 26, line 30; figures 1-15	1,2,30, 34
A	US 5 823 942 A (MASAHIRO TOHIDA) 20 October 1998 (1998-10-20) see the whole document; figures 1-14	1,2,30, 34

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☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

25 July 2000

Date of mailing of the international search report

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Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

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Visser, F

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/CA 99/01174

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
WO 9732182 A	04-09-1997	AU 1977597 A EP 0883793 A JP 2000503237 T US 5956355 A	16-09-1997 16-12-1998 21-03-2000 21-09-1999
WO 9922198 A	06-05-1999	NONE	
US 5823942 A	20-10-1998	JP 3000320 B JP 6063048 A JP 3000321 B JP 6063049 A JP 2981700 B JP 6070881 A US 5716324 A US 5810719 A	17-01-2000 08-03-1994 17-01-2000 08-03-1994 22-11-1999 15-03-1994 10-02-1998 22-09-1998

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